



NOVEMBER 7, 13, & 20, 2024

# Evolution of Structures

Steel Castings in the Eye of the Design Team

Featuring Speakers from:

**ELENA**  **M<sup>de</sup>AS**

**Severud Associates**  
CONSULTING ENGINEERS P.C.

*Industry leaders use steel castings to turn bold visions into reality.*

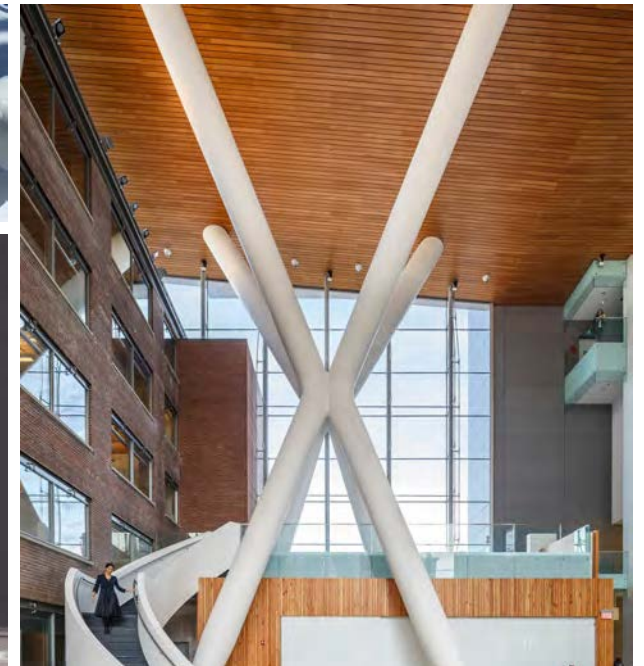


# CASTCONNEX<sup>®</sup>

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We simplify the design and enhance the performance of structures by enabling Architects and Engineers to use cast steel connections.

We take pride in collaborating in the creation of safer, innovative, and more beautiful built environments.





# Evolution Structures

Steel Castings in the Eye of the Design Team

## Longueuil Downtown TOD

An Innovative Urban Center

CASTINGS301-24 | 1LU/HSW | Live Webinar | Introductory | Prerequisites: None  
AIA CES PROVIDER NUMBER:404108320

### Speaker:

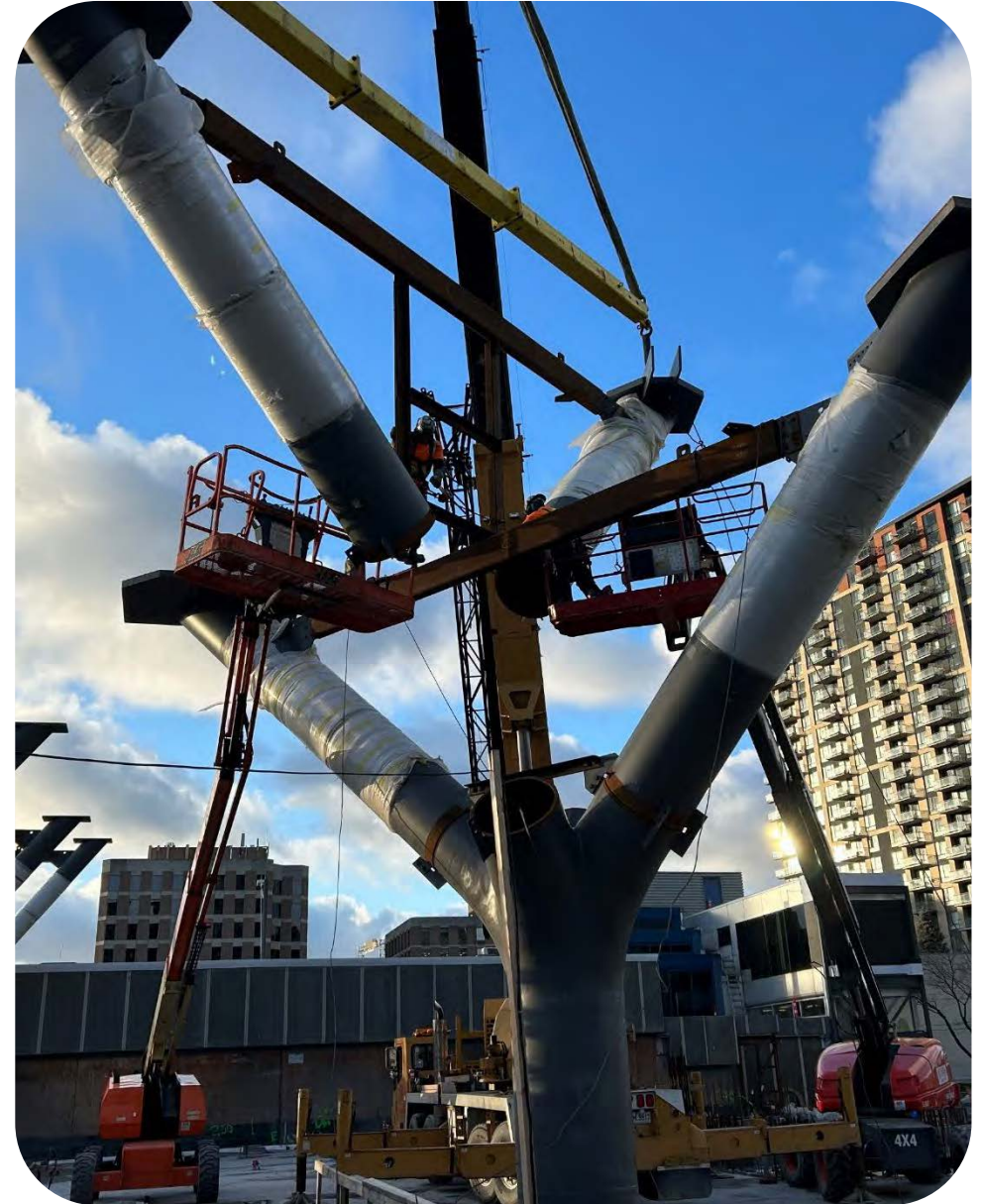
**Félix Bédard, M.Eng., P.Eng.**  
Vice President & Co-Founder | Elema

**ELEMA**

### Moderator:

**Tarana Haque, M.A.Sc, P.Eng.**  
Technical Sales Manager, North  
America | CAST CONNEX

 **CAST  
CONNEX®**



## COURSE DESCRIPTION

This presentation will explore the design and engineering of the Longueuil Downtown Lot 2 project, which is part of a multi-million-dollar real estate development for the city's transit-oriented development (TOD) initiative – an upcoming urban centre in the Greater Montreal region. This project is made up of two 33-storey residential towers, each located on either side of the Longueuil–Université-de-Sherbrooke metro terminal tunnel. Its podium feature allows the towers above to overhang the infrastructures of the tunnels and platforms of the metro station while providing access for STM (Société de transport de Montréal) transit users to the station below. To provide commercial space and a food court in the podium feature, the design includes impressive “tree-shaped” steel structures which span the tunnels and platforms of the metro station below.

In this presentation, learn about the design and engineering of this project, along with the challenges of building over an existing transit line. Learn how the design team incorporated flexible design practices to account for existing yet imprecise infrastructure. Explore the architectural programming and how the architecturally exposed structural steel (AESS) trees complete with custom-designed cast steel nodes enabled large free-spans and architecture for commercial space and access for transit users to the metro tunnels and platform.

## LEARNING OBJECTIVES

1. Understand how the design and construction of the towers and podiums met the architectural and structural goals set by the project stakeholders: the city, the metro, and the developer.
2. Explore the flexible design methods the engineer of record used to adapt for the on-site imprecise or unknown geometry of existing infrastructure.
3. Quantify the effects of laying new foundations from existing metro installations from complex geotechnical and geomechanical studies.
4. Investigate how the architecturally exposed structural steel (AESS) trees with cast steel nodes support free-space architecture in the podium, enabling long spans for the food court and commercial area.



# SUMMARY

- **Location:** Longueuil, Canada
- **Years:** 2018 – On going
- **Development value:** \$500 million
- **Scale:** total area of 1.2 million square feet
- 1,200 housing units
- Nearly 60 000 square feet of commercial/public space
- Development sits on top of a STM subway station
- Neighbours ARTM public transit terminal
- Direct access to Sherbrooke University's Longueuil campus

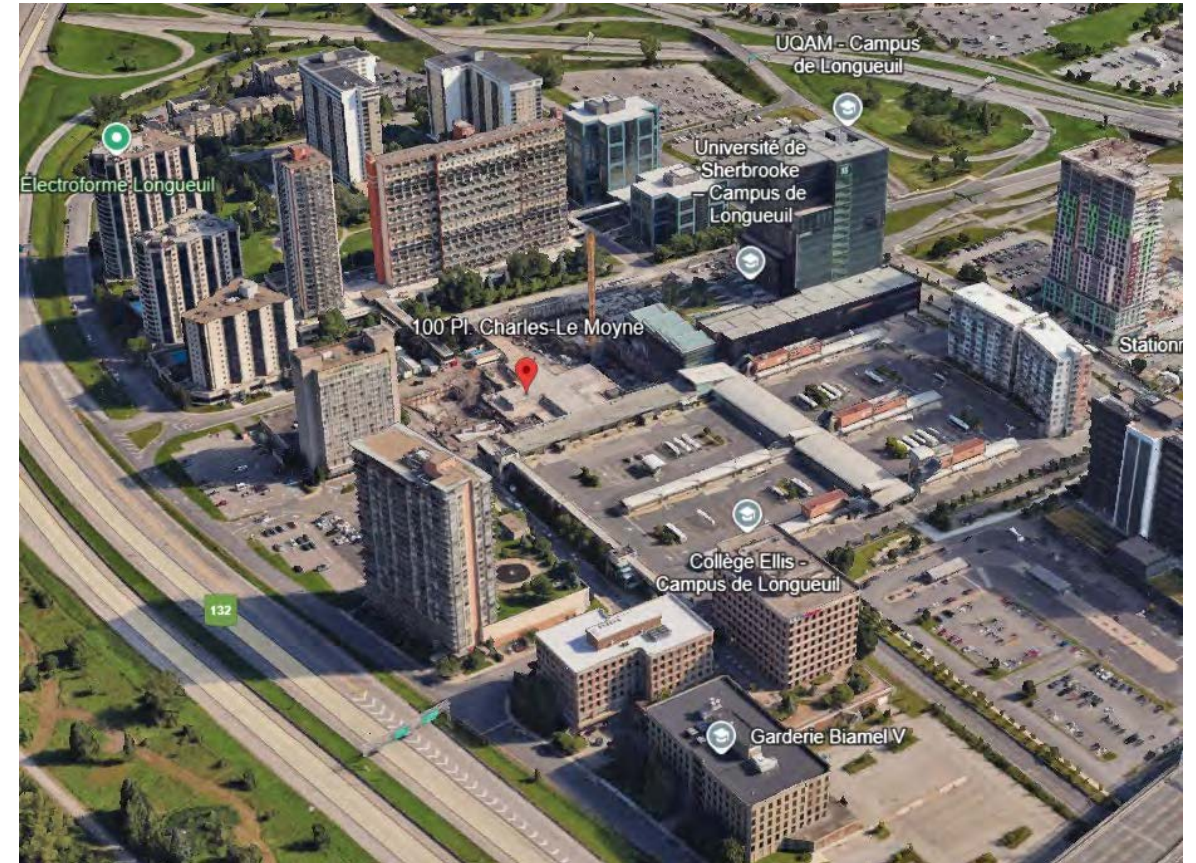
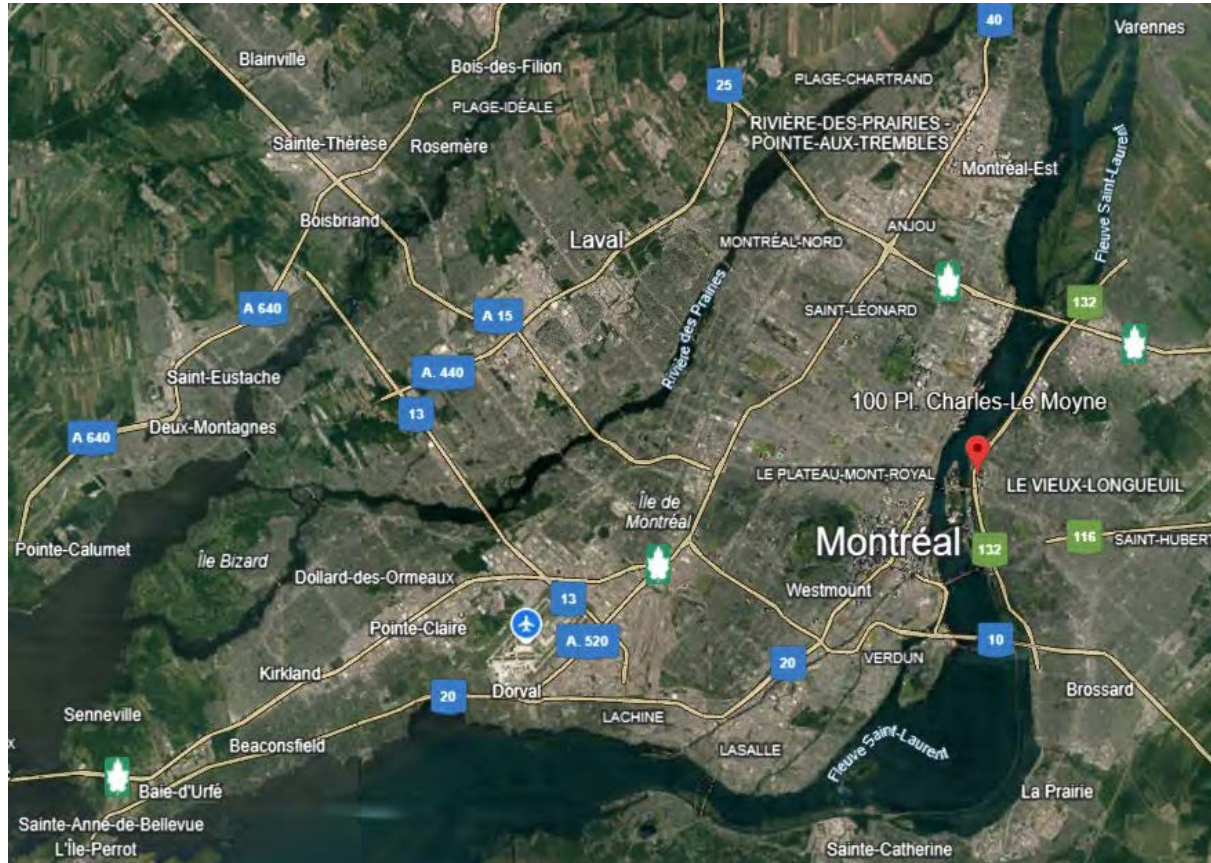




# PROJECT CONTEXT, SITE AND HISTORY



# CONTEXT





# CONTEXT

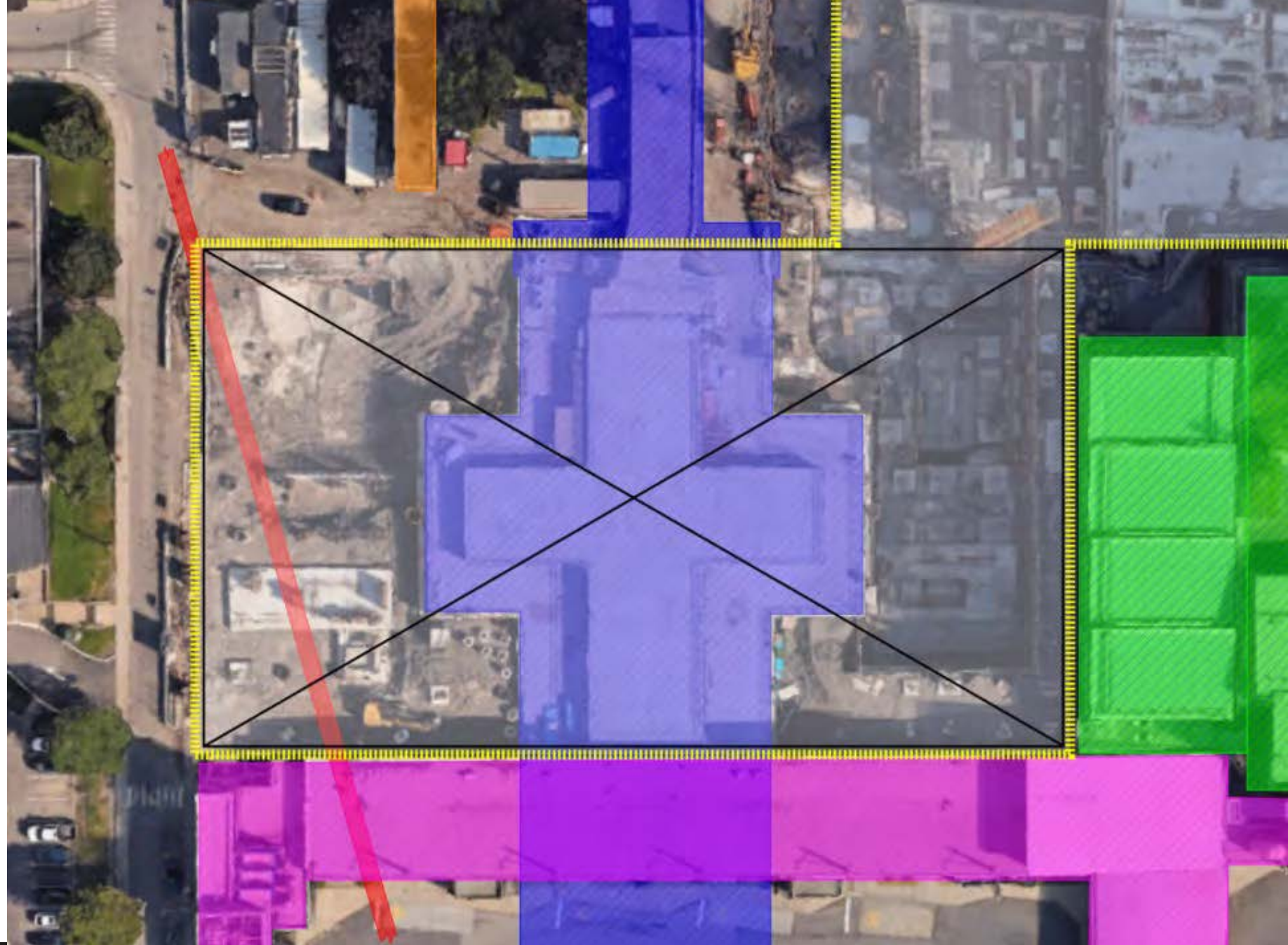
- PROJECT SITE

STM SUBWAY

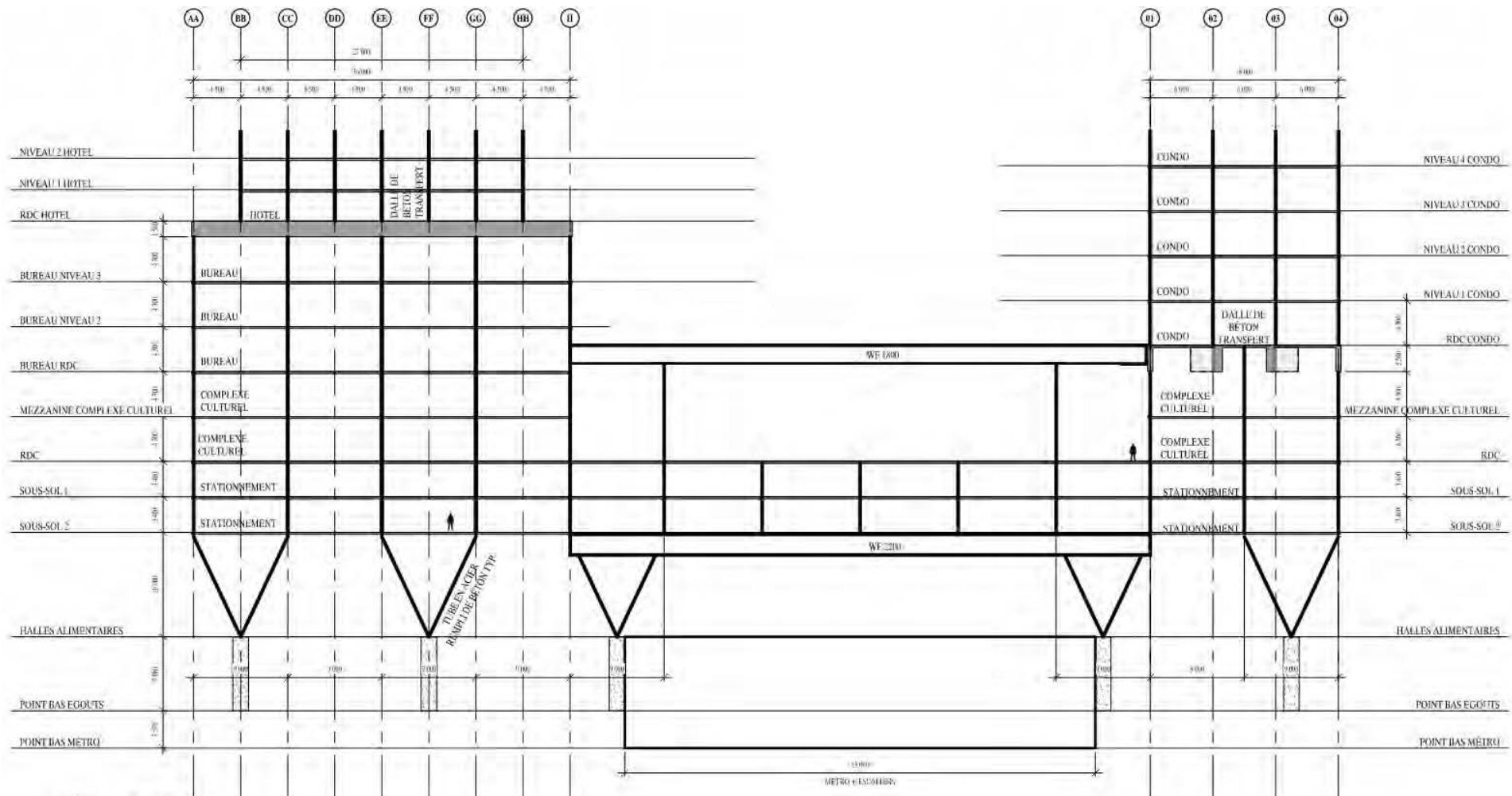
- ARTM BUS TERMINAL

- SHERBROOKE UNIVERSITY

- UNDERGROUND  
DRAINAGE LINE



# EVOLUTION OF THE PROJECT



1 COUPE  
Éch.: 1 : 350

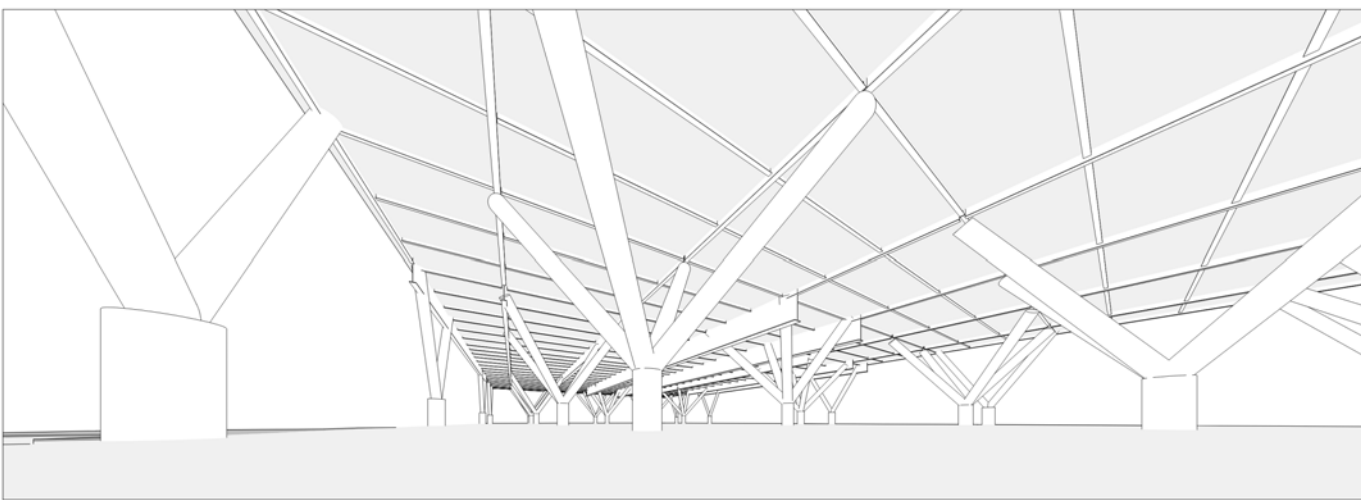
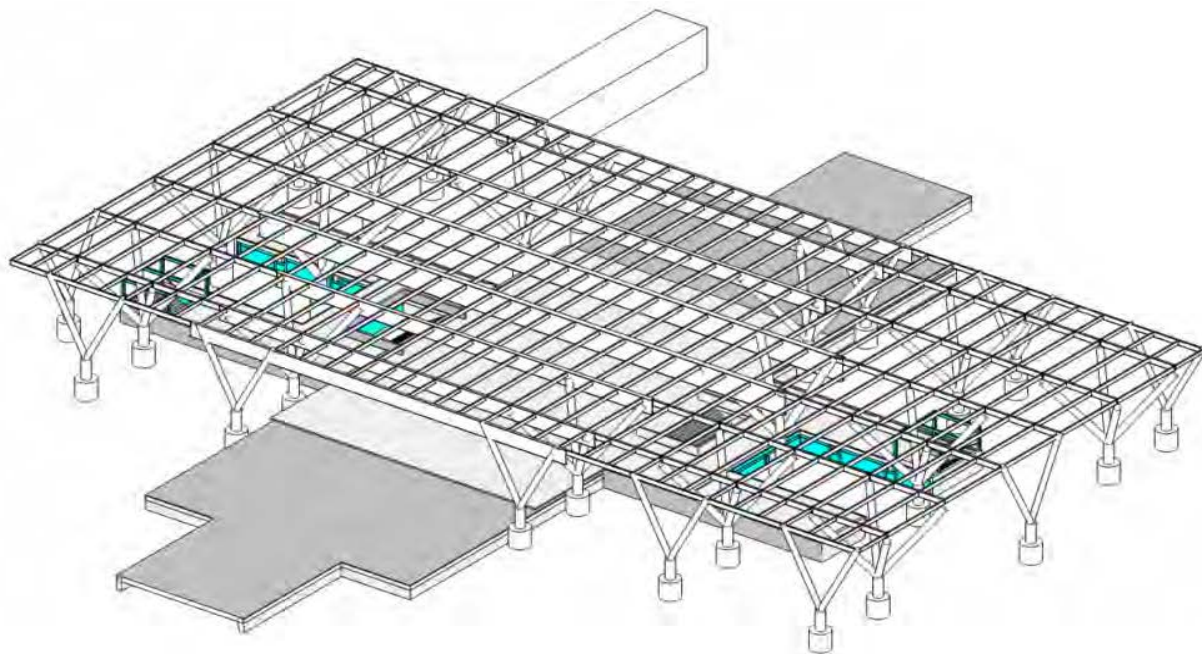
PROPOSITION STRUCTURALE

JUIN / 2018



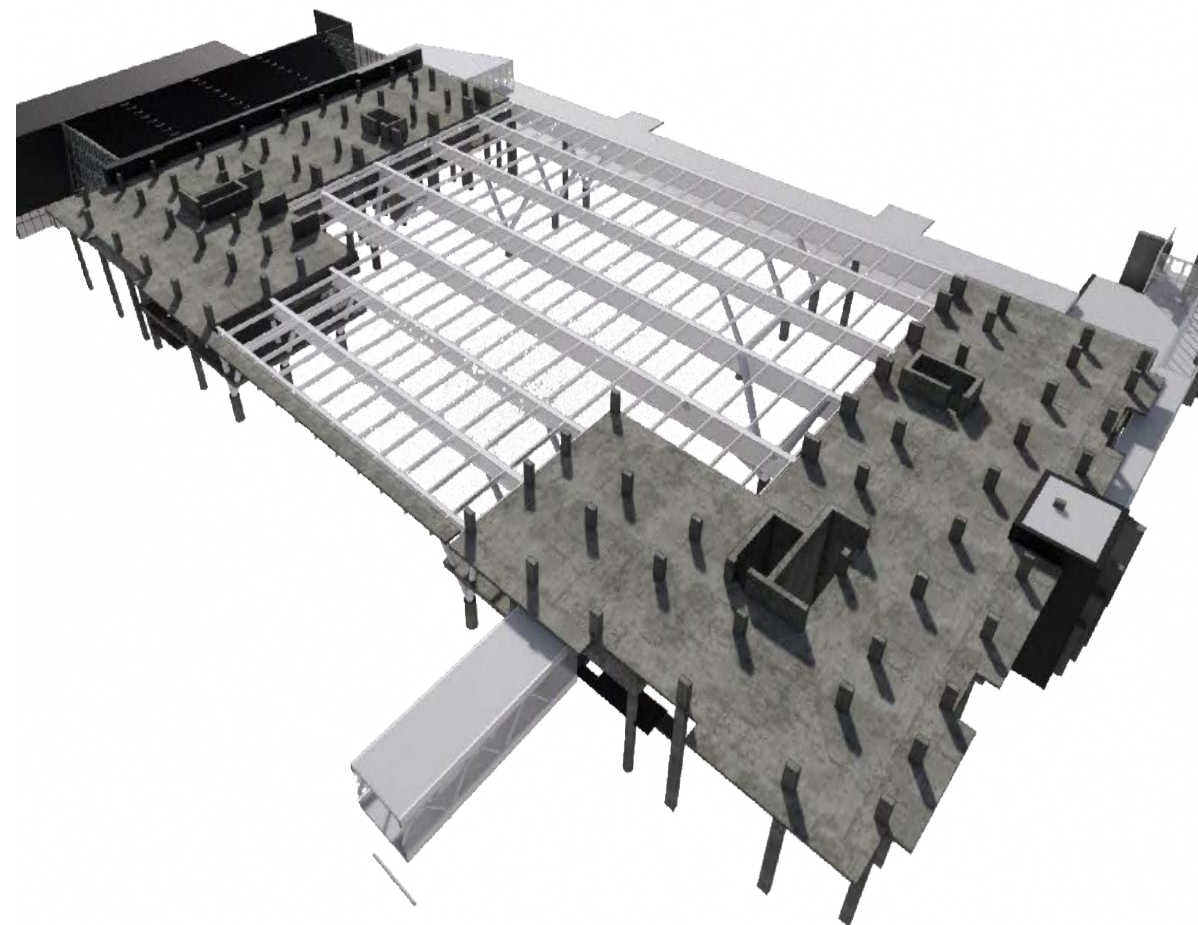


# EVOLUTION OF THE PROJECT





# EVOLUTION OF THE PROJECT

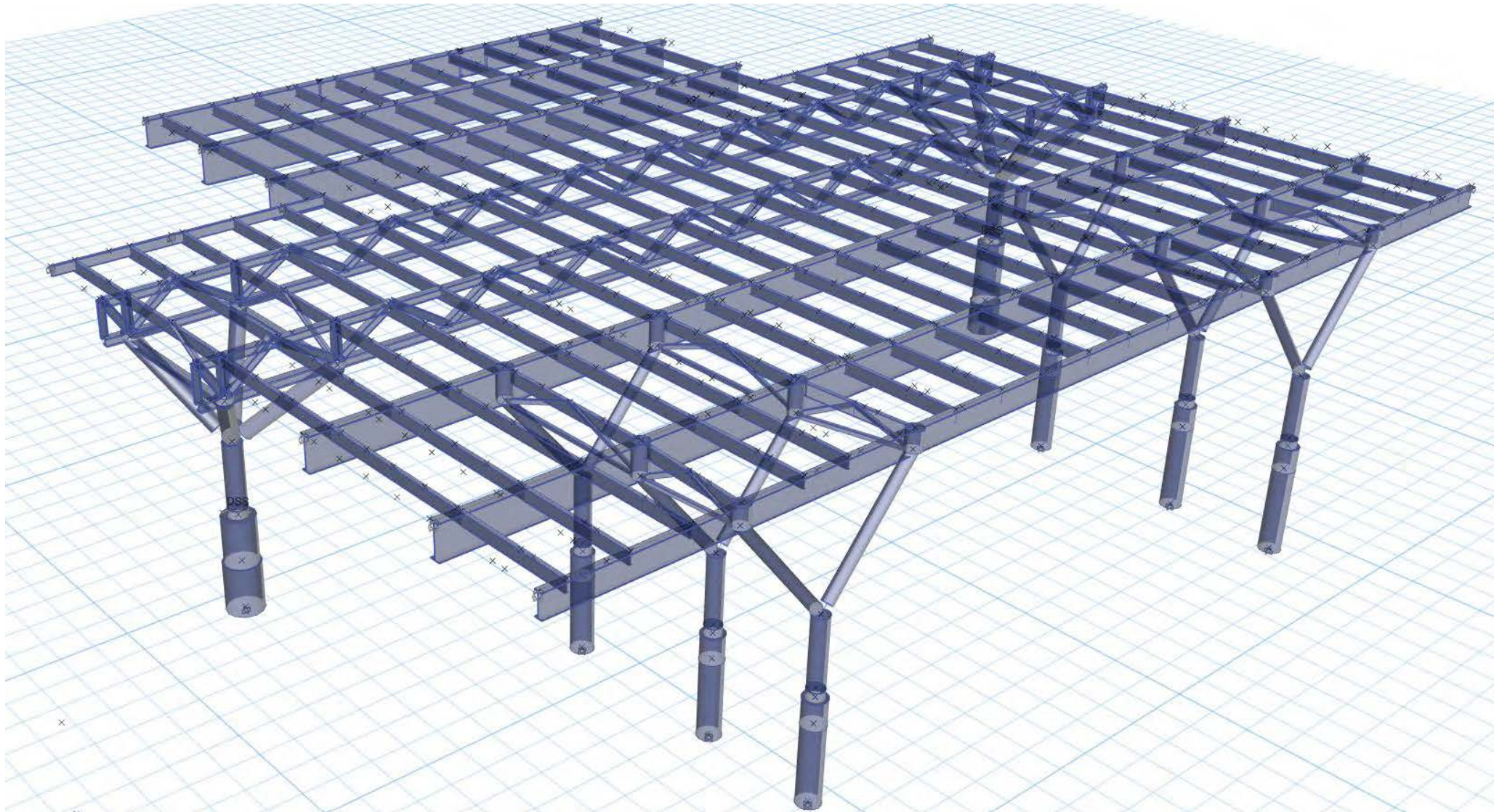




# STRUCTURAL DESIGN

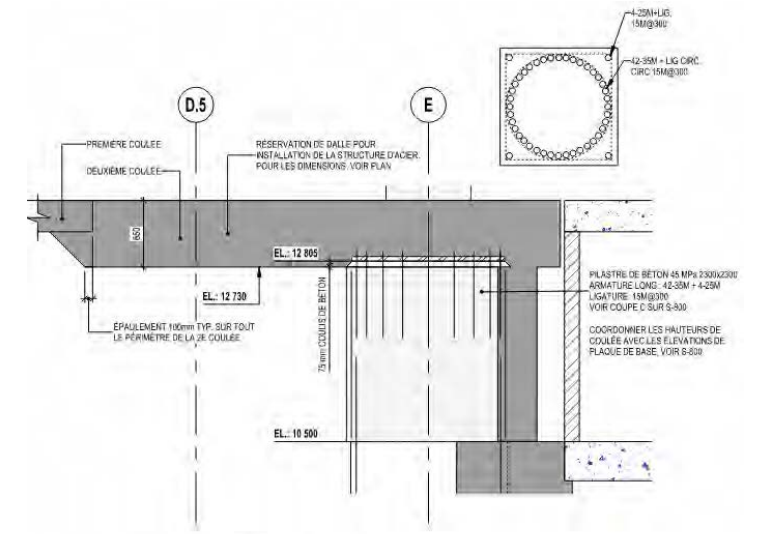
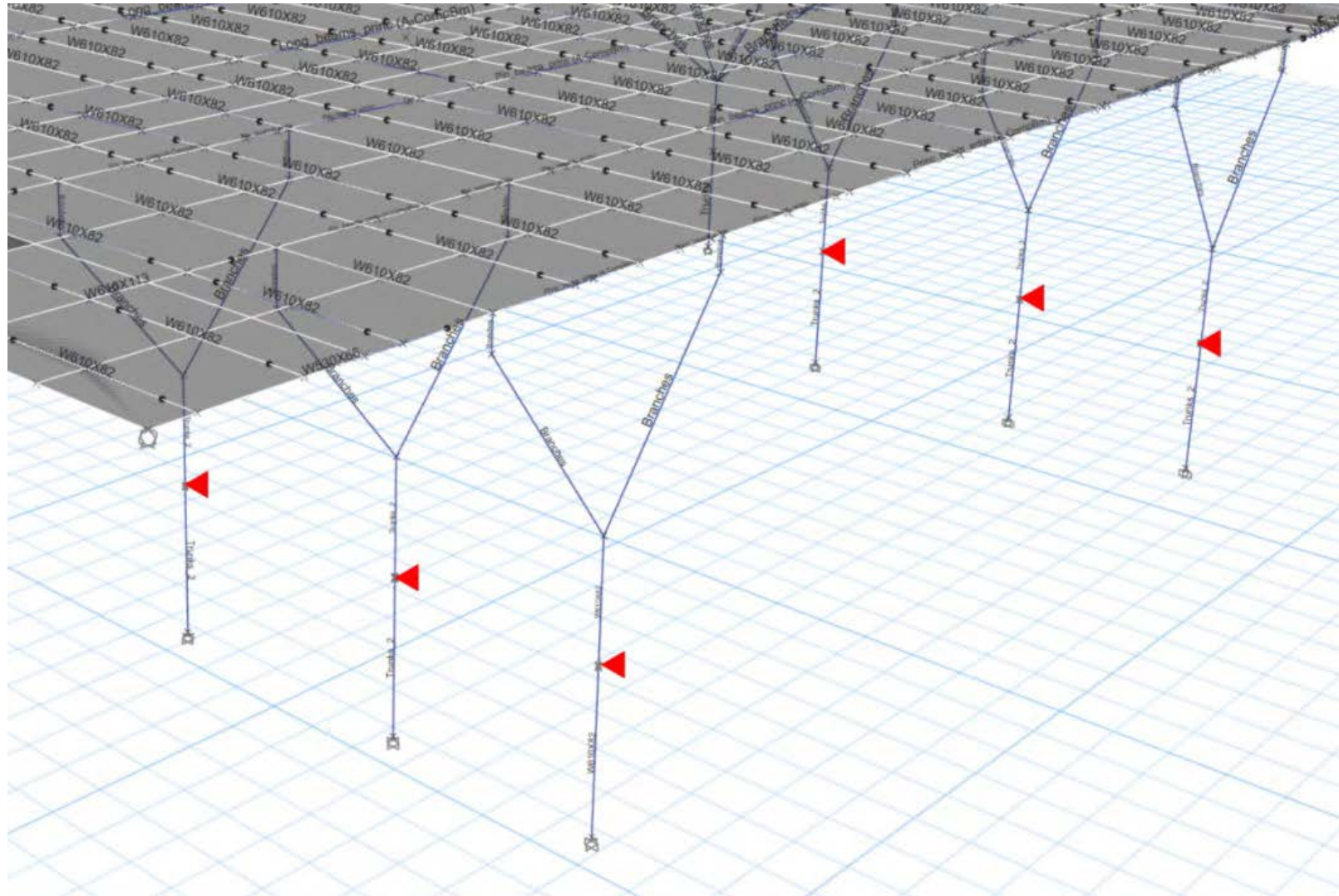


# STRUCTURAL MODELING

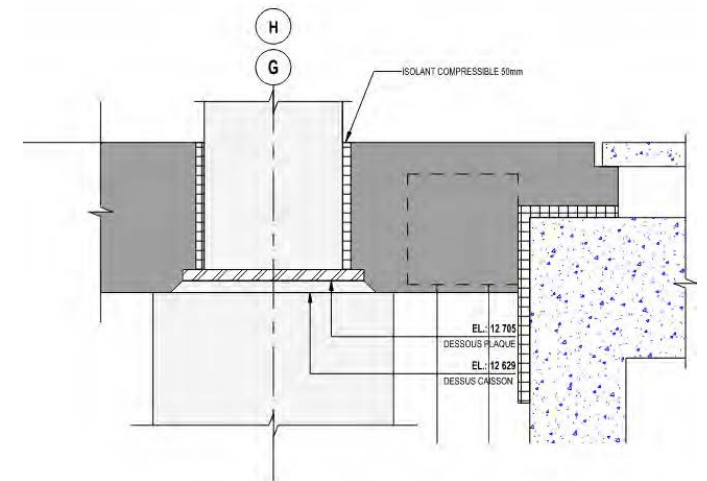




# STRUCTURAL MODELING



**2 COUPE**  
S-090 Éch.: 1 : 50



**8 COUPE**  
S-090 Éch.: 1 : 25

# STRUCTURAL MODELING

## DESIGN ACCORDING TO CNBC/CCQ 2010 & 2015 – DIVISION B PART 4

Province: QC - Québec

City: Brossard

Select "Custom site" at the end of the cities list to customize the spectral acceleration. See note (3) to obtain custom Canadian spectral acceleration.

Site class: NBC 2010 - 4.1.8.4 2) et 3) C

$S_a(0.2)$

0,640 g

$S_a(0.5)$

0,310 g

$S_a(1.0)$

0,140 g

$S_a(2.0)$

0,047 g

PGA

0,330 g

$F_a$

1,000

$F_v$

1,000

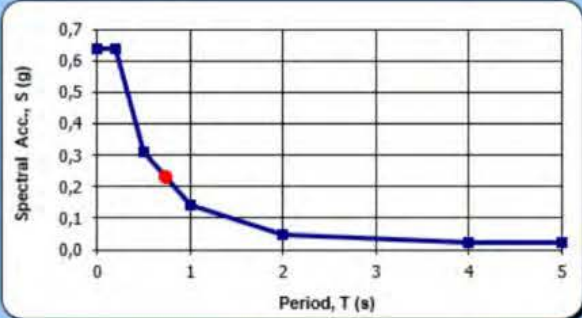
Spectral acceleration at fundamental period:

$S(T_a)$

0,2244 g

Period, T (s)

Spectral Acc., S (g)



$T \leq 0.2$  s

0,6400 g

$T = 0.5$  s

0,3100 g

$T = 1.0$  s

0,1400 g

$T = 2.0$  s

0,0470 g

$T \geq 4.0$  s

0,0235 g

CNBC 2005 - 4.1.8.4 6)

Lateral Fundamental Period

Type of building: Steel moment frames

Empiric formula used: NBC 2010 - 4.1.8.11 3) a) b) et c)

$T_a$  emp.

0,5011 s

$T_a = 0,085 h_n^{3/4}$

☒ Mechanical method NBC 2010 - 4.1.8.11 3) d)

$T_a$  méca.

0,7623 s

PERIOD IN Y DIRECTION: 1.96 sec.

< Enter the period

$T_a =$

0,7517 s

NBC 2010 - 4.1.8.11 3)

The fundamental period is limited to 1,5x the fundamental period determined with the NBC 2010 empirical formula.

Force Modification Factors

CSA standard used: Steel Structures -- Standard CSA-S16 NBC 2010 - 4.1.8.9

$R_d$

1,5

$R_o$

1,3

SFRS: Conventional construction of moment-resisting frames, braced frames or plates walls - Assembly occupancies

Building Parameters

Risk category: Normal NBC 2010 - 4.1.8.5

$I_E$

1,0

Building height:  $H_n$  10,65 m

Number of storeys:  $N$  1

Higher Mode Effects

Type of seismic force resisting system: Moment-resisting frames

$S_a(0.2)/S_a(2.0)$

13,617

$M_v$

1,000

$J$

0,950

Design Lateral Earthquake Force at the Base

$V = S(T_a) M_v I_E W / (R_d R_o) =$

0,1151 W

$V_{min} = S(2.0) M_v(2.0) I_E W / (R_d R_o) =$

0,0289 W

$V_{max} = (2/3) S(0.2) I_E W / (R_d R_o) =$

0,2188 W

Min. lateral seismic force: NBC 2010 - 4.1.8.11 2)

$V$

0,1151 W

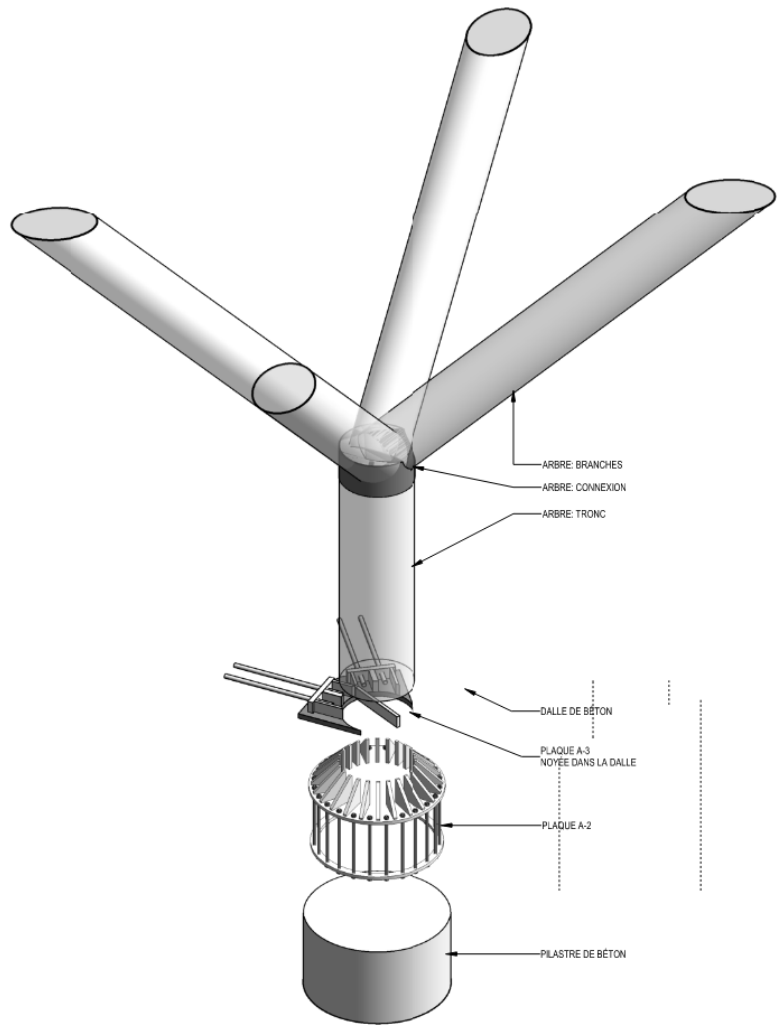
Check the restrictions of page 3

ELEMA

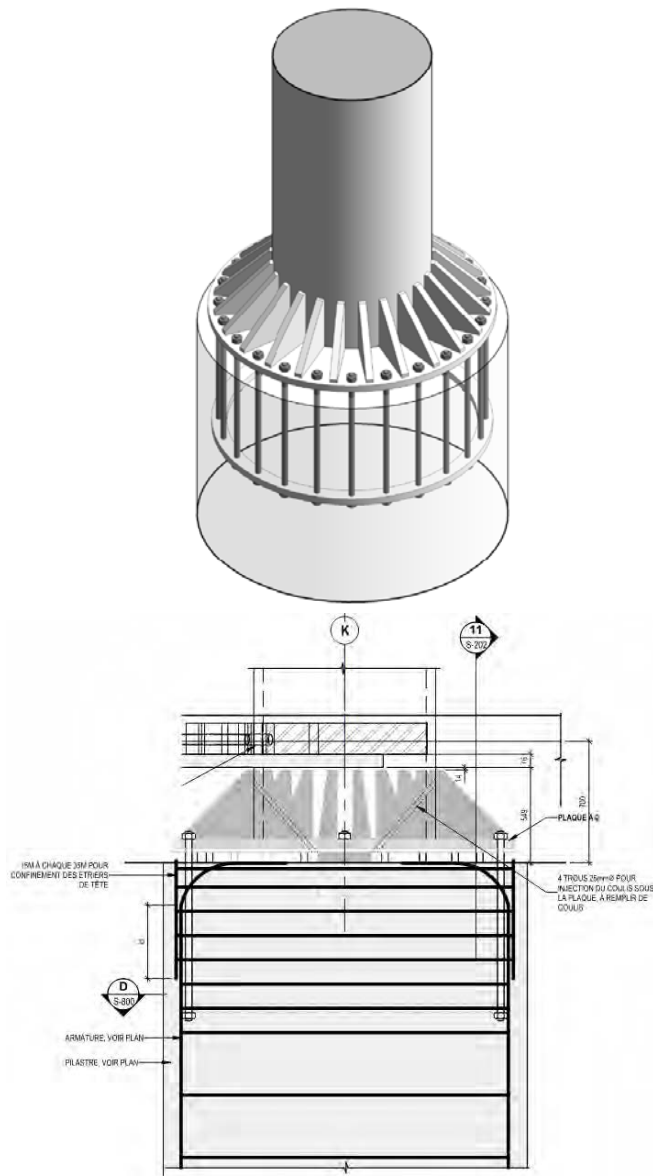
CASTCONNEX



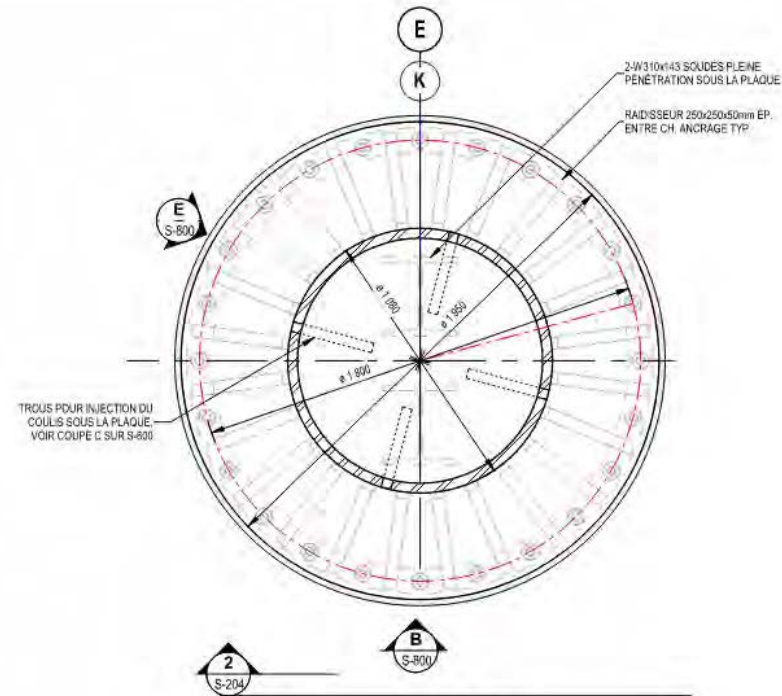
# DETAILED DESIGN



VUE 3D DES ARBRES ET CONNEXIONS DÉPLOYÉES



C COUPE  
S-800  
Éch.: 1 : 20

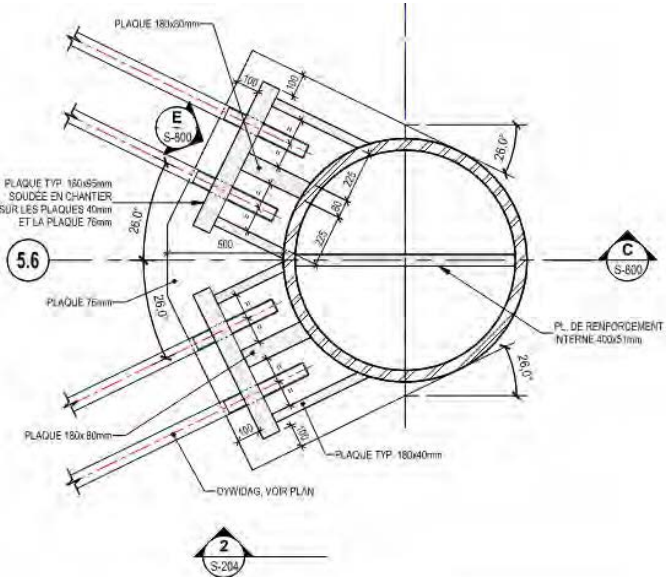
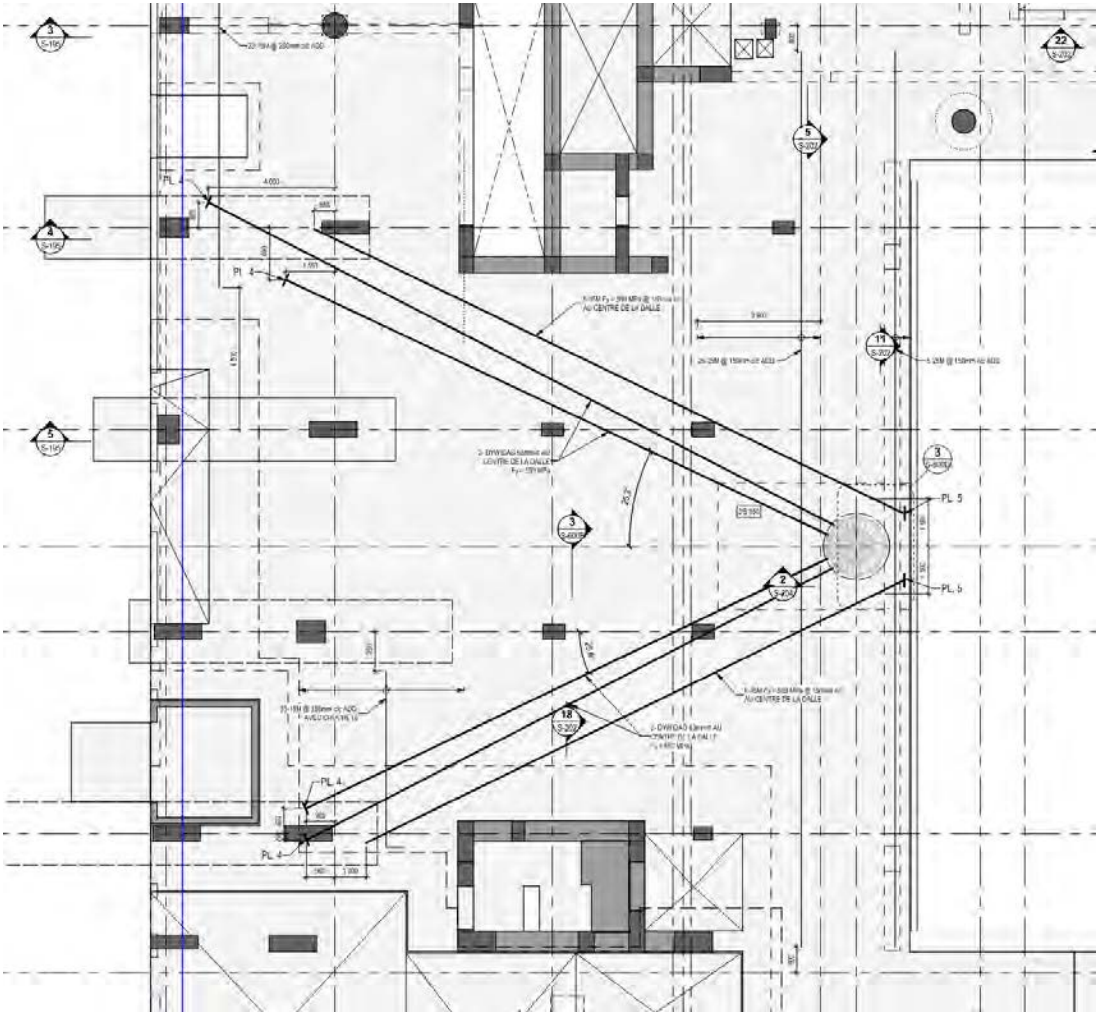


PL - A2	
PLAQUE	1950mm DIA. x 50mm ÉP. 345 MPa
ANCRAGES	24 x 44mm DIA. ENF. 1150mm + 2-W310x143 250mm LG.
ELEVATION DESSOUS PLAQUE DE BASE	12 805

TOUTES PLAQUES 345 MPa S.I.C.  
ANCRAGES TYPE F3125-150 AVEC  $F_{tk} = 1040 \text{ MPa}$

Anchor patterns:  
24 x 44mm dia (1,75in)

# DETAILED DESIGN



2  
S-204

## PL - A3

PLAQUE	76 mm
ANCRAGES	VOIR PLAQUE A2

TOUTES PLAQUES 345 MPa S.I.C.





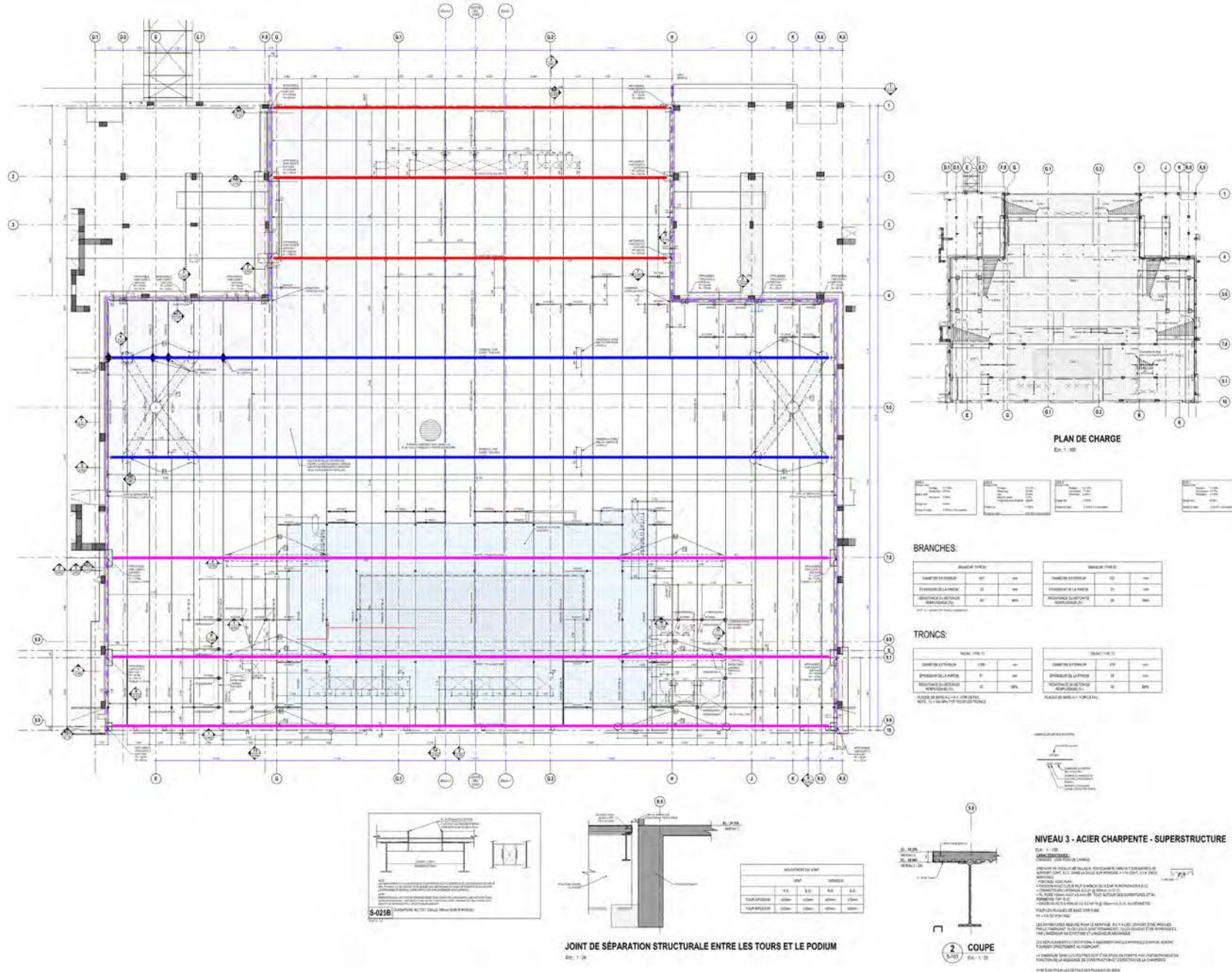
# DETAILED DESIGN





# DETAILED DESIGN

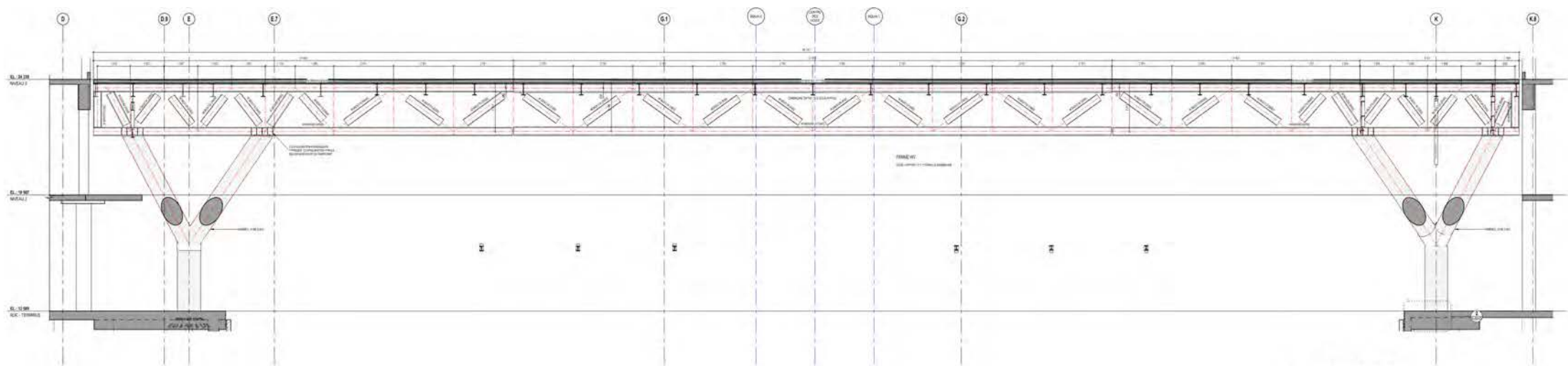
- 8 main members
- 140-210mm composite slab on deck



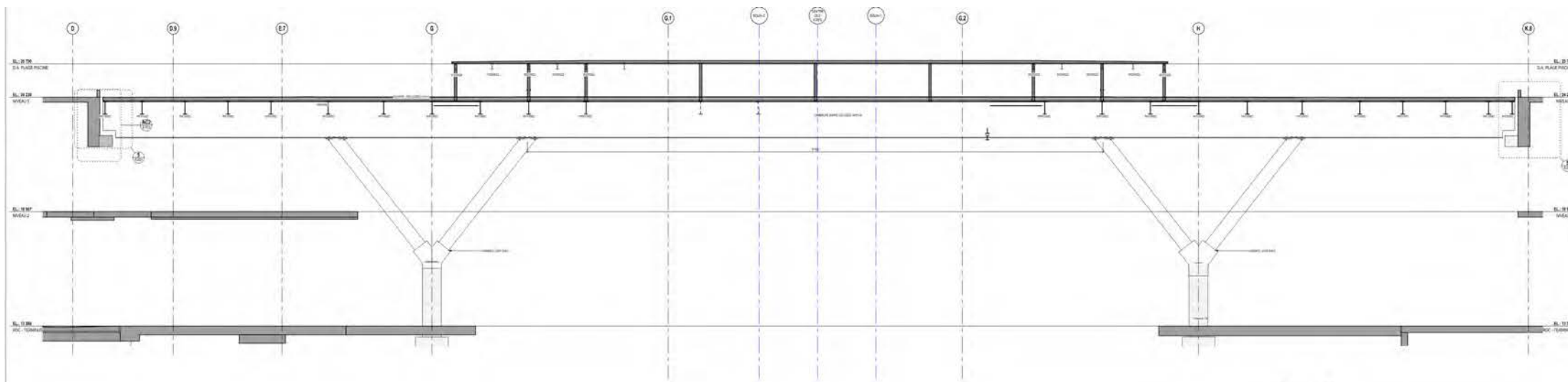


# DETAILED DESIGN

Warren Truss : 2400mm deep (8ft), max span 57,5m (189ft)



1 COUPE (FERME W2)  
Ech. 1/50



2 COUPE  
Ech. 1/50

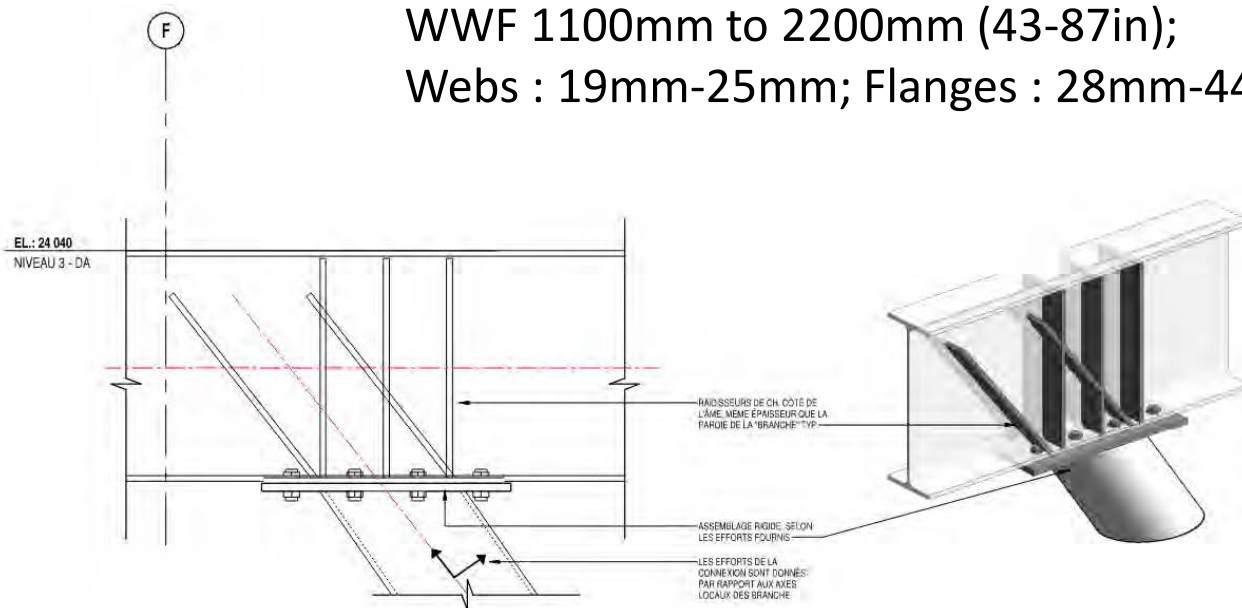
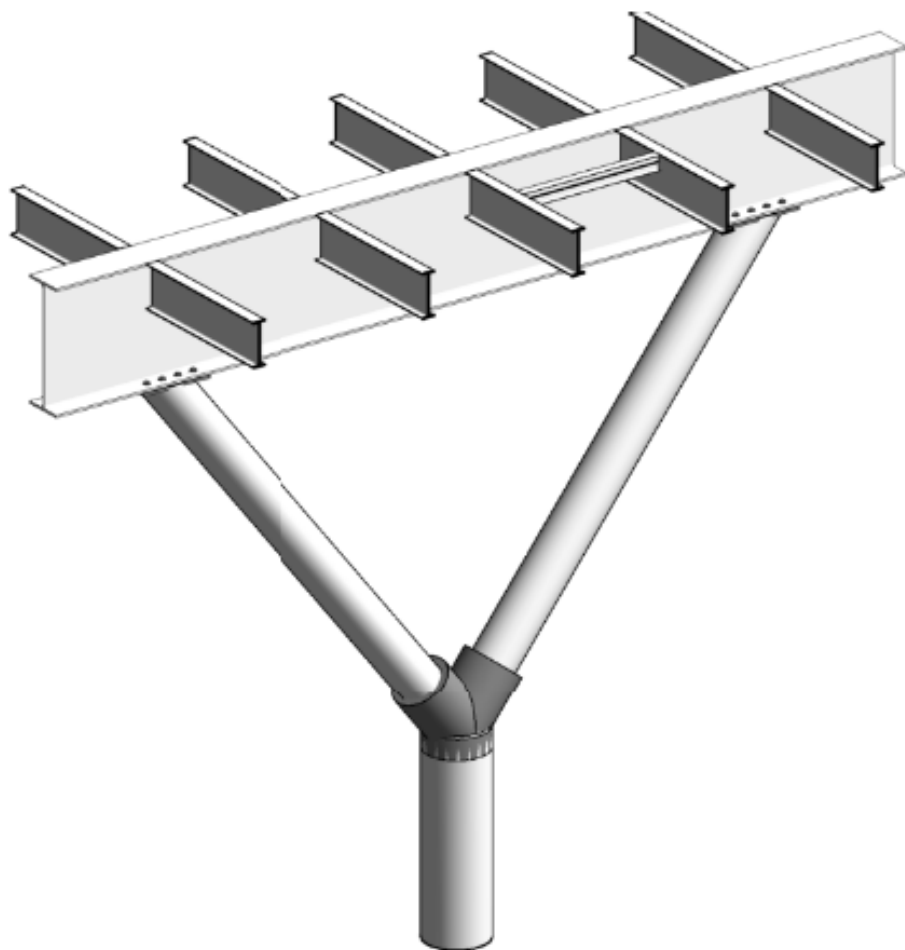






# DETAILED DESIGN

WWF 1100mm to 2200mm (43-87in);  
Webs : 19mm-25mm; Flanges : 28mm-44mm



NOTES :

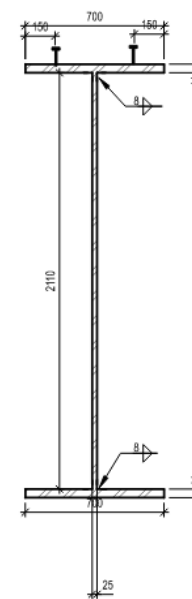
- TOUS LES ASSEMBLAGES DOIVENT ÊTRE ENTièrement CONÇUS PAR LE FABRICANT (NOMBRE DE ROLLONS À TITRE INDICATIF SEULEMENT)
- LES ARBRES (TRONC ET BRANCHES) DOIVENT AVOIR UN DEGRÉ DE FINITION ARCHITECTURALE AESS 2, INCLUANT LES ASSEMBLAGES
- AVANT LA SOUMISSION DES DESSINS D'ATELIER, LE FABRICANT D'ACIER DEVRA FOURNIR UNE SÉRIE DE CROQUIS MONTRANT LES DÉTAILS D'ASSEMBLAGE DES ARBRES (TRONC ET BRANCHES) AVEC NOTES DE CALCULS COMPLÈTES. CES CROQUIS FERMONT L'OBJET D'UN EXAMEN DE L'INGÉNIEUR EN STRUCTURE AINSI QUE DE L'ARCHITECTE QUI SE RÉSERVE LE DROIT D'EXIGER DES AJUSTEMENTS, NOTAMMENT POUR LES CONNEXIONS ARCHITECTURALES, DANS LE BUT DE RESPECTER L'INTENTION VISUELLE.

5

S-802

CONNEXION TYPIQUE BRANCHE/POUTRE

Éch.: 1:20

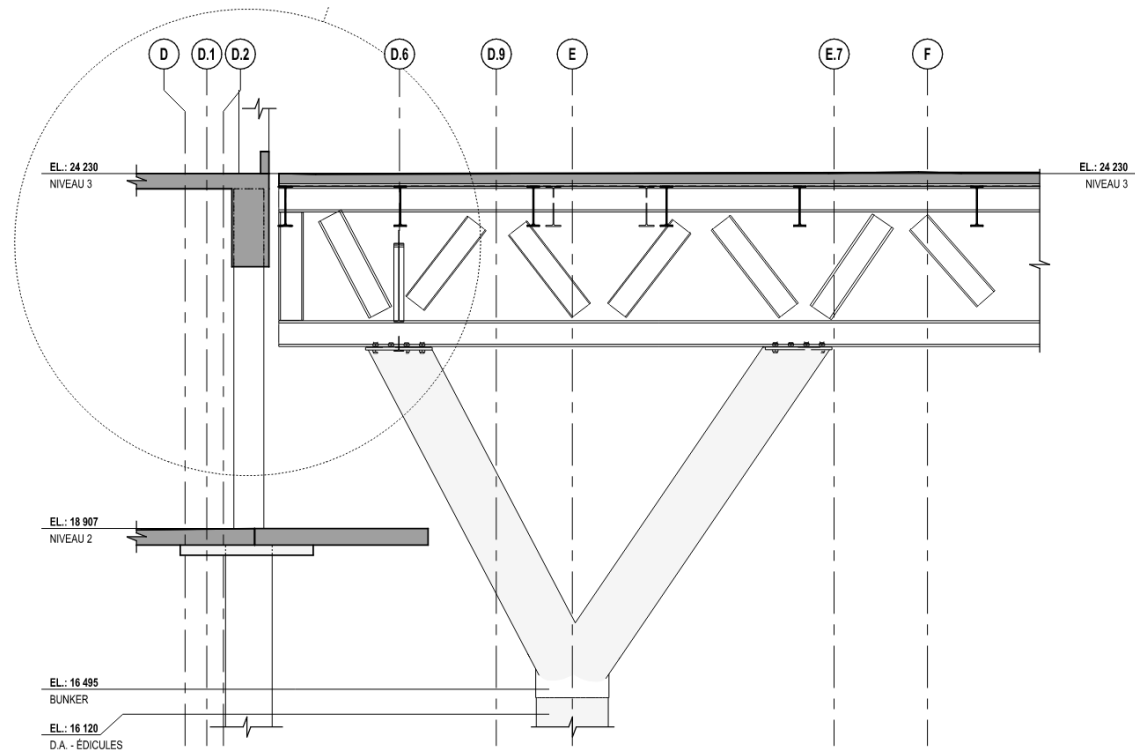


W1

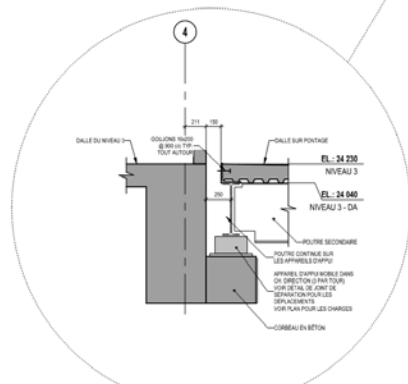
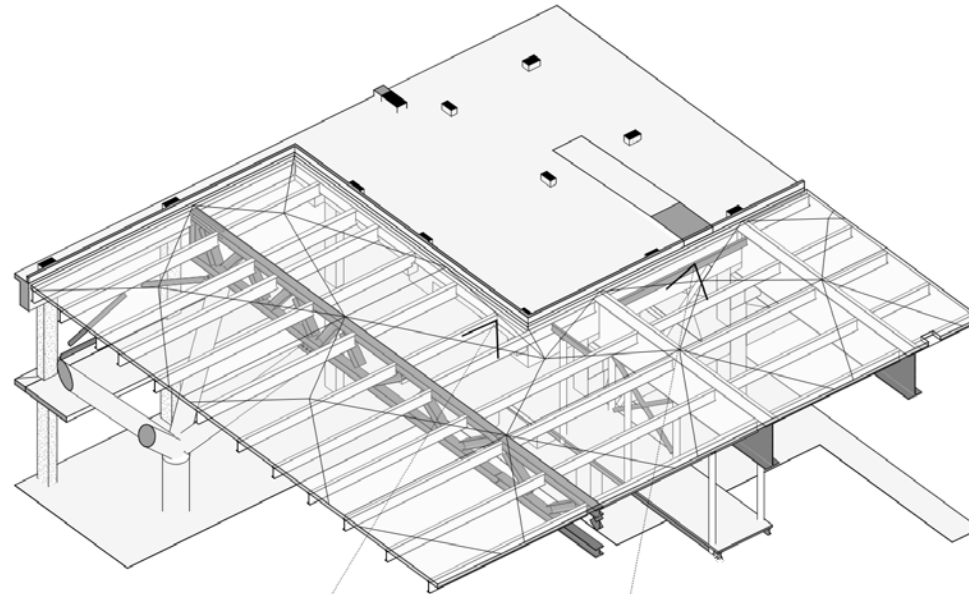
VUE 3D DES ARBRES DES AXES 7.8 ET 9.1



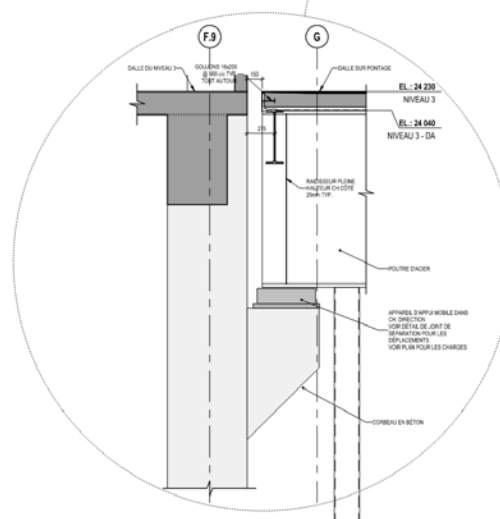
# DETAILED DESIGN



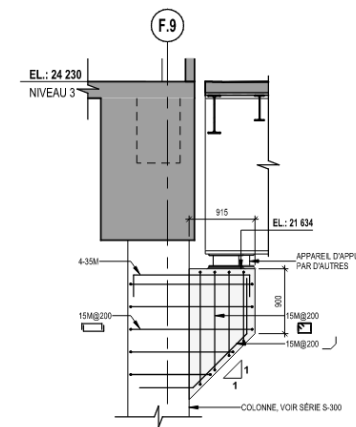
**1 COUPE**  
Éch.: 1:50



**3 COUPE C**  
S-801 Ech.: 1:25



**2 COUPE B**  
S-801 Ech.: 1:25



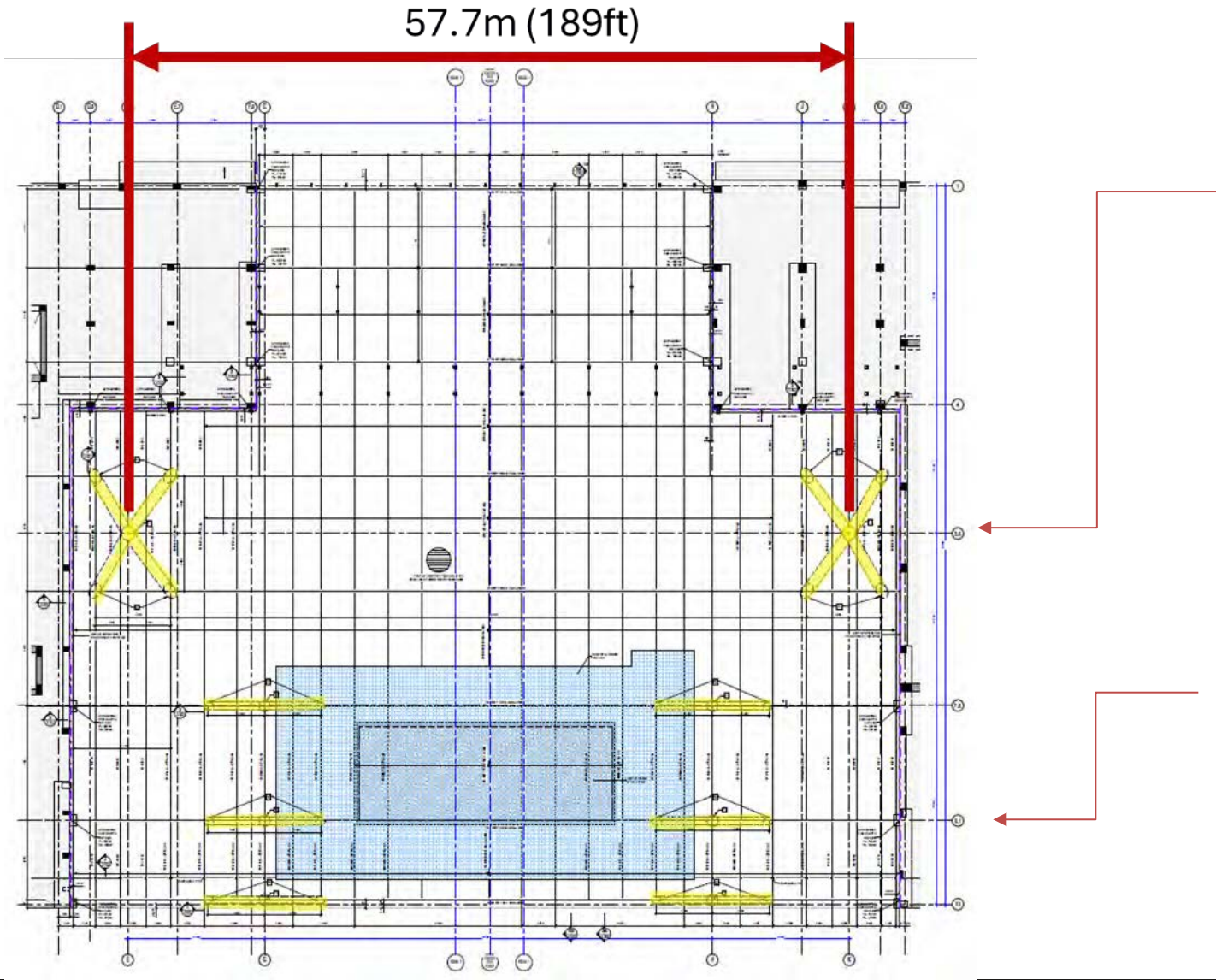
**AB COUPE**  
S-103 Ech.: 1:50



# ELEMA & CAST CONNEX COLLABORATION



# CONTRACT DOCUMENTS

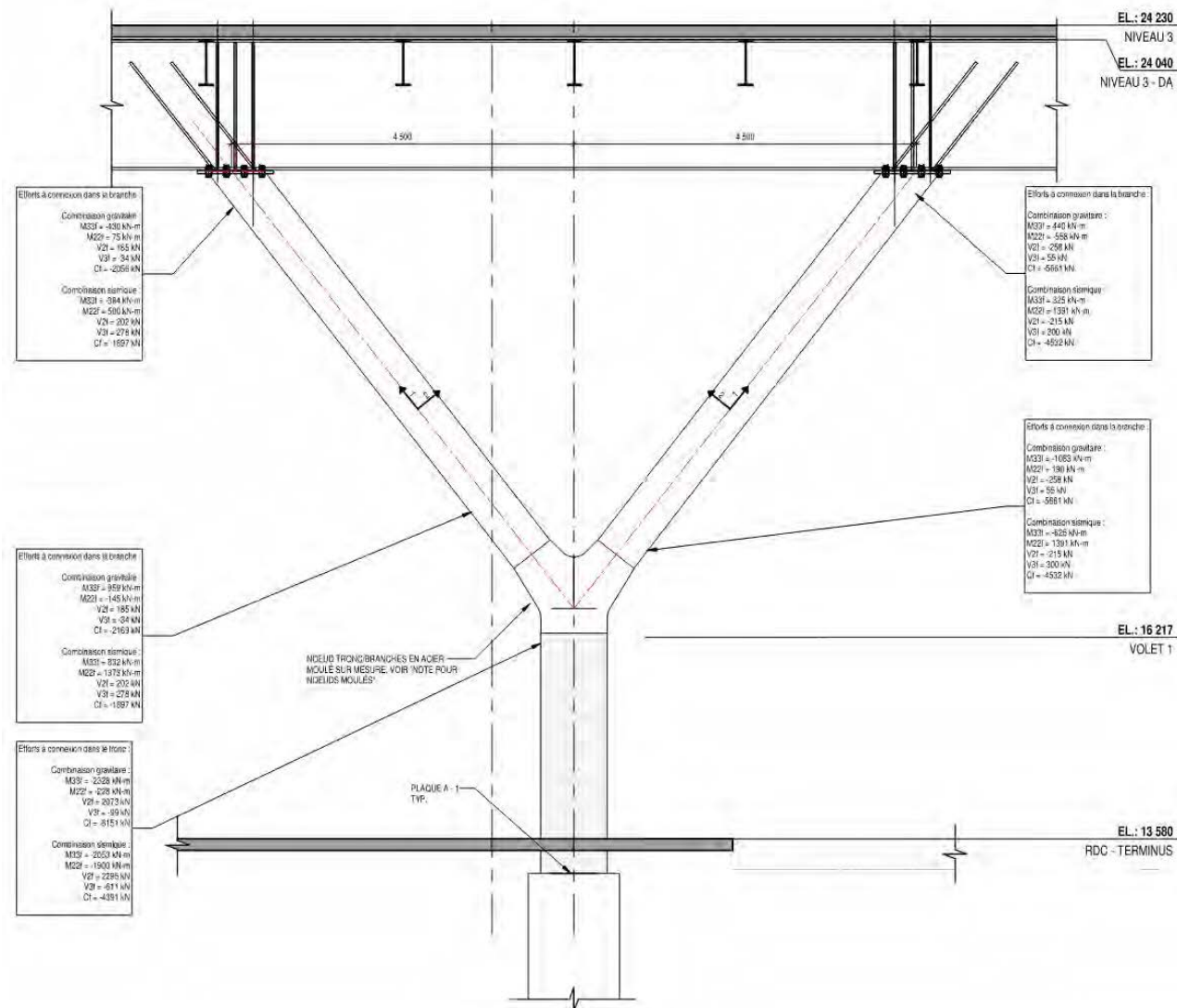
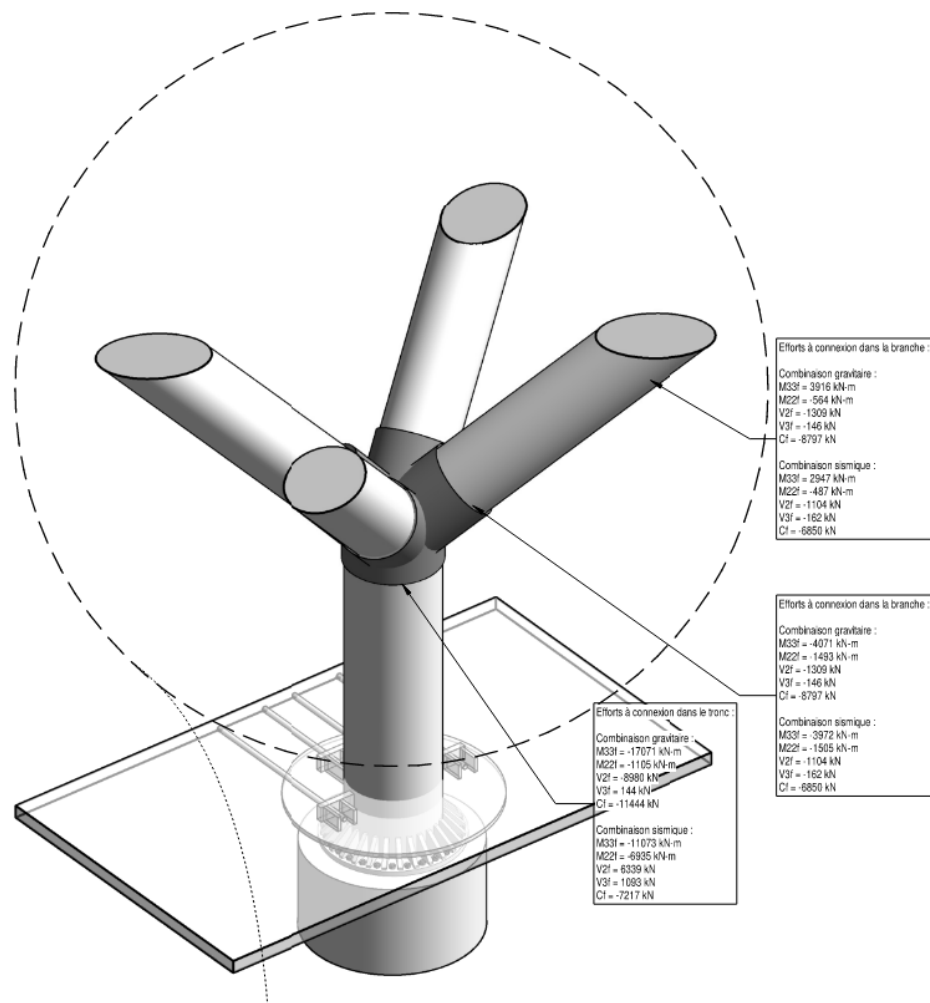


2 x Tree Nodes*	OD x t (mm)
Trunk	1050 x 48
Branch (4)	850 x 32

6 x Y-Nodes*	OD x t (mm)
Trunk	875x 28
Branch (2)	600 x 25

\* Concrete-filled,  $f'_c = 40 \text{ MPa}$

100



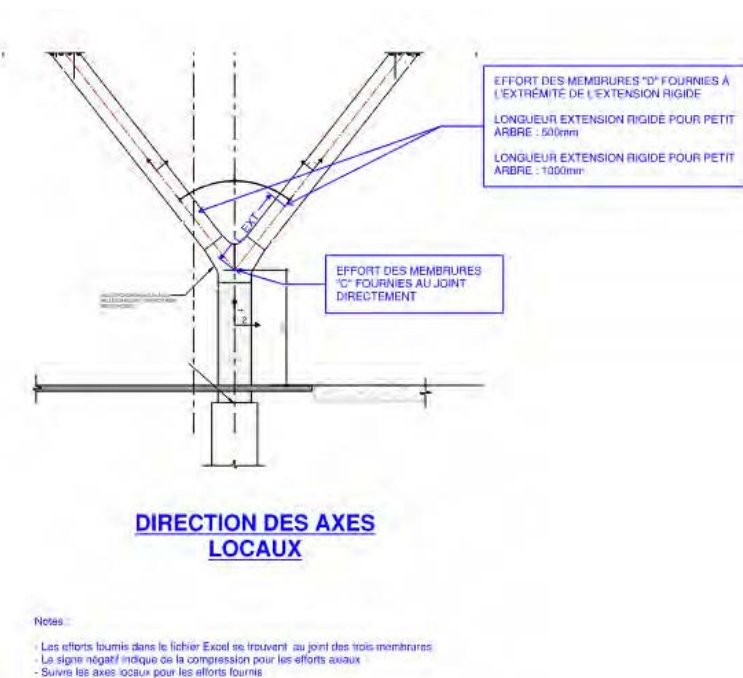
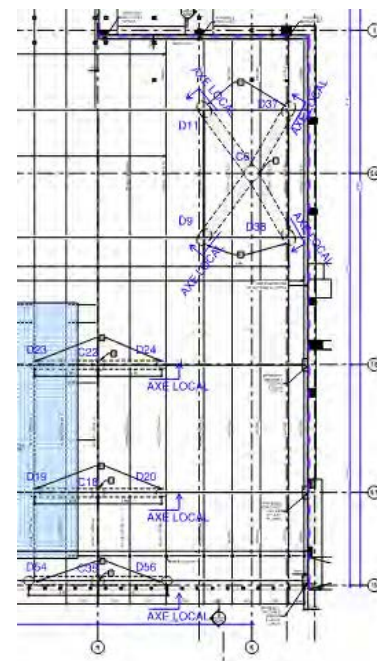
**2** **COUPE B**  
S-099 Éch.: 1 : 50

NOTE :  
LES ARBRES (TRONC ET BRANCHES) DOIVENT  
AVOIR UN DEGRÉ DE FINITION ARCHITECTURAL  
AESS 2, INCLUANT LES ASSEMBLAGES



100

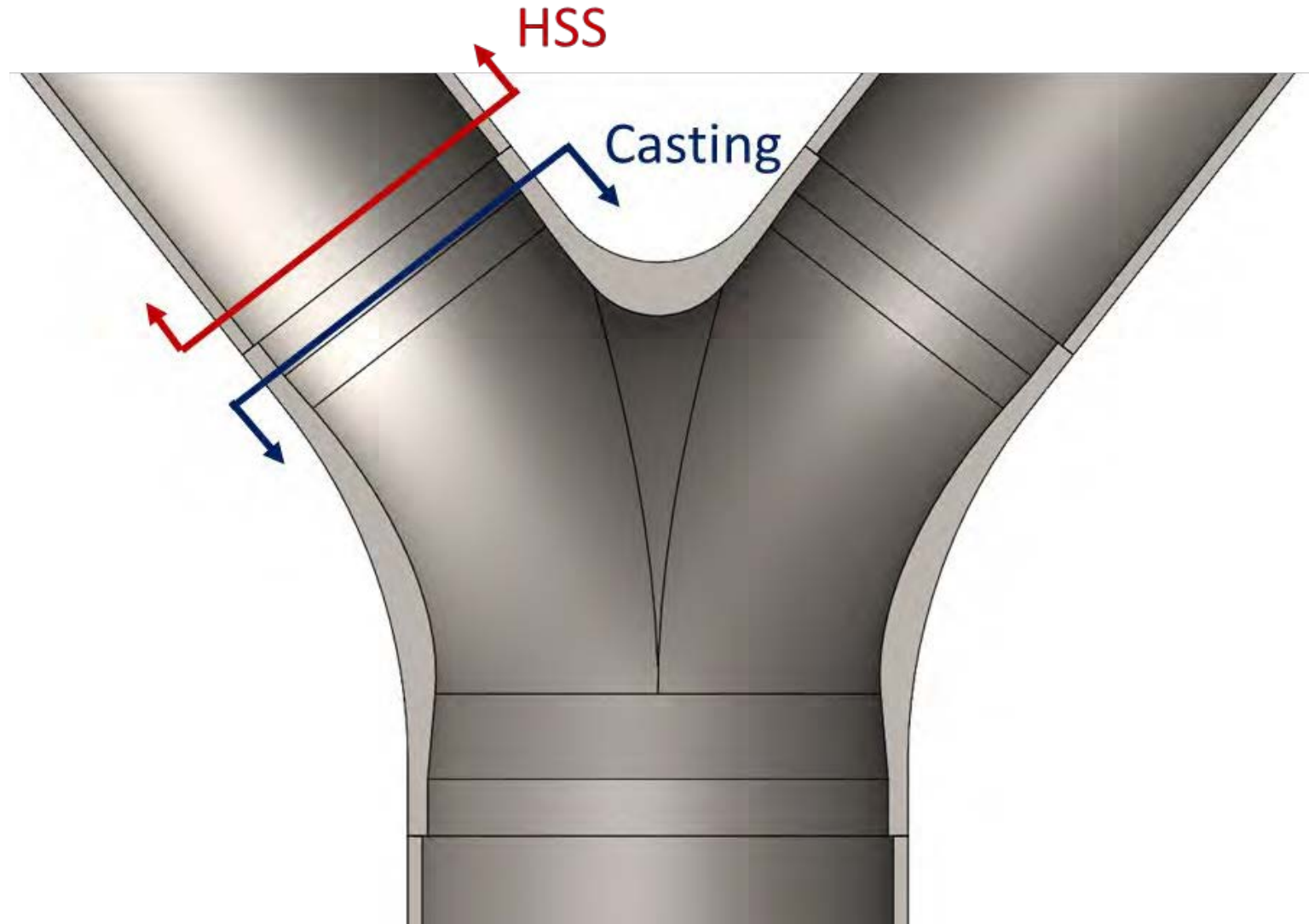
Colonne	Cas de chargement	Modèle	Step Typ	P kN	V2 kN	V3 kN	T kN-m	M2 kN-m	M3 kN-m
C13	1.25D+1.25SD+1.5L	1		-6178	-724	-63	-91	-10	2718
C18	1.25D+1.25SD+1.5L	1		-6181	703	-55	99	2	-2747
C21	1.25D+1.25SD+1.5L	1		-6549	-803	-19	7	-123	3017
C22	1.25D+1.25SD+1.5L	1		-6572	770	-14	5	-111	-3025
C35	1.25D+1.25SD+1.5L	1		-2207	358	-50	92	-2	-1325
C5	1.25D+1.25SD+1.5L	1		-10094	-7511	115	-29	-1361	15168
C6	1.25D+1.25SD+1.5L	1		-10144	7557	125	69	-1180	-15246
C7	1.25D+1.25SD+1.5L	1		-2208	-349	-57	-85	-17	1267
C13	1.25D+1.25SD+1.5L	2		-6109	-910	-70	-91	-42	2750
C18	1.25D+1.25SD+1.5L	2		-6113	881	-59	102	-23	-2807
C21	1.25D+1.25SD+1.5L	2		-6466	-1010	-20	11	-136	3051
C22	1.25D+1.25SD+1.5L	2		-6492	961	-13	4	-118	-3084
C35	1.25D+1.25SD+1.5L	2		-2183	422	-53	96	-25	-1255
C5	1.25D+1.25SD+1.5L	2		-10093	-7507	124	-25	-1296	15169
C6	1.25D+1.25SD+1.5L	2		-10146	7569	136	72	-1102	-15216
C7	1.25D+1.25SD+1.5L	2		-2187	-405	-61	-86	-46	1178
C13	1.25D+1.25SD+1.5L	3		-6178	-724	-63	-90	-10	2717
C18	1.25D+1.25SD+1.5L	3		-6181	704	-55	99	2	-2748
C21	1.25D+1.25SD+1.5L	3		-6548	-803	-19	7	-123	3016
C22	1.25D+1.25SD+1.5L	3		-6572	770	-14	5	-111	-3026
C35	1.25D+1.25SD+1.5L	3		-2207	359	-51	92	-2	-1325
C5	1.25D+1.25SD+1.5L	3		-10095	-7331	116	-29	-1353	15606
C6	1.25D+1.25SD+1.5L	3		-10143	7375	124	69	-1181	-15651
C7	1.25D+1.25SD+1.5L	3		-2209	-349	-57	-85	-17	1266
C13	1.25D+1.25SD+1.5L	4		-6109	-909	-70	-91	-42	2747
C18	1.25D+1.25SD+1.5L	4		-6112	882	-60	102	-24	-2810
C21	1.25D+1.25SD+1.5L	4		-6466	-1008	-20	11	-135	3046
C22	1.25D+1.25SD+1.5L	4		-6491	964	-14	3	-119	-3089
C35	1.25D+1.25SD+1.5L	4		-2184	423	-54	95	-26	-1255
C5	1.25D+1.25SD+1.5L	4		-10094	-7331	126	-28	-1279	15631
C6	1.25D+1.25SD+1.5L	4		-10145	7385	134	69	-1111	-15677

[illegible]

# DESIGN OF CAST STEEL NODES

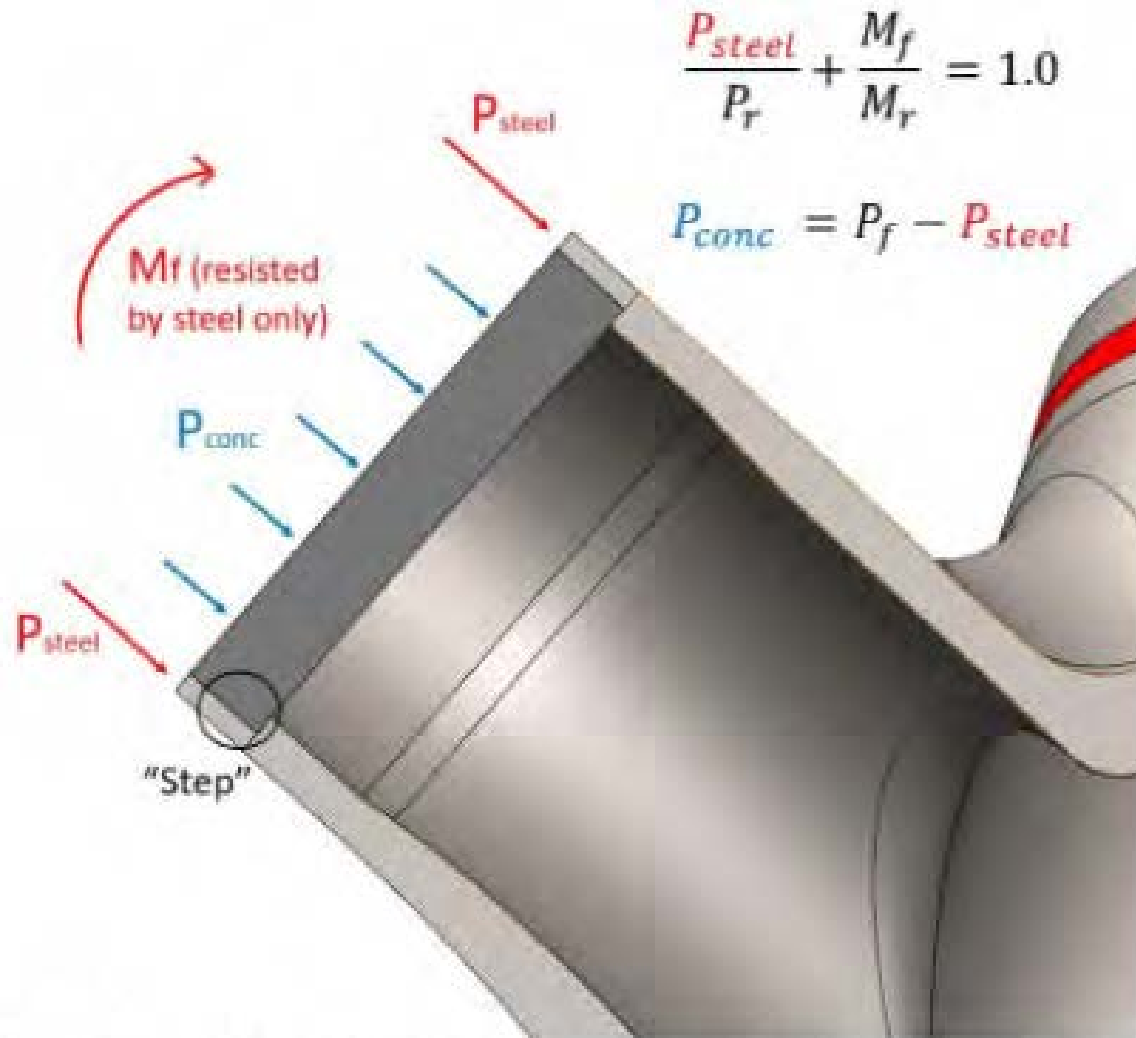
Preliminary sectional analysis:

- Does the incoming HSS member rely on the concrete inside to resist the load? **YES**
- Can the custom casting be designed to carry the loads alone without considering concrete? **YES**
- How can we develop an analysis model to find a possible load path that allows loads carried by the concrete filled HSS to be transferred into the casting?





# DESIGN OF CAST STEEL NODES



Assume:

- The HSS member takes the full applied bending with additional axial loads until its utilization factor reaches 1.0.
- The remaining axial load will be carried by the concrete and transfer to the casting through the internal "step" without crushing the concrete.

Figure 9. Established load path from concrete filled HSS to casting body

# DESIGN OF CAST STEEL NODES

CASTCONNEX <sup>®</sup>					
Project: Edyfic Place Charles-Lemoyne				Project No. P21-111	No. 11 of 19
Design: FW	Drawn: FW	Checked: MGG	Date: July 06, 2022	W.P. No.	Scale N.T.S.
Subject: Cast Steel Nodes for Edyfic Place Charles-Lemoyne – Engineering Report				Reference:	

Table 2: Geometry properties and factored resistance of attached HSS members

Node Type	Member	Diameter (mm)	Design Thickness (mm)	Pr = φAFy (kN)	Mr = φMp (kN*m)
EPCL-01 (Tree-Node)	B1 (branch)	850.9	31.75	25369	6618
	T1 (column)	1079.5	50.8	50975	16705
EPCL-02 (Y-Node)	B2 (branch)	596.9	25.4	14159	2577
	T2 (column)	876.3	25.4	21082	5711

## 4.2.1 Example Calculation of Utilization Factor

To demonstrate the calculation of utilization factors, Table 3 lists one set of loading information at the interface between column member C5 and node EPCL-01. Evaluating this set of loads against the factored resistance of member “T1” included in Table 2, it is demonstrated that member “T1” will not be over-utilized in this particular case.

Table 3: Processed loading information at the interface between member C5 and EPCL-01

Member	Load Combination	Mode	P (kN)	F2 (kN)	F3 (kN)	T (kN*m)	M2 (kN*m)	M3 (kN*m)
C5	1.25D+1.25SD+1.5S	1	9919	6937	-38	-40	-449.4	-9151.1

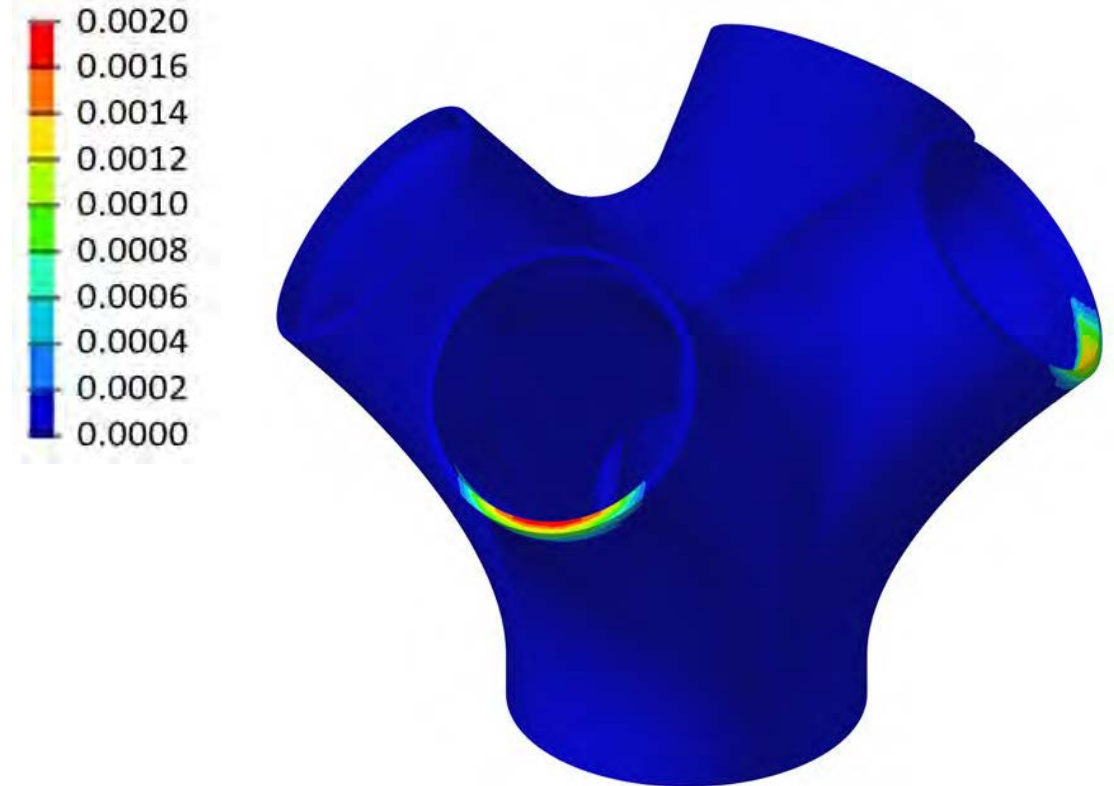
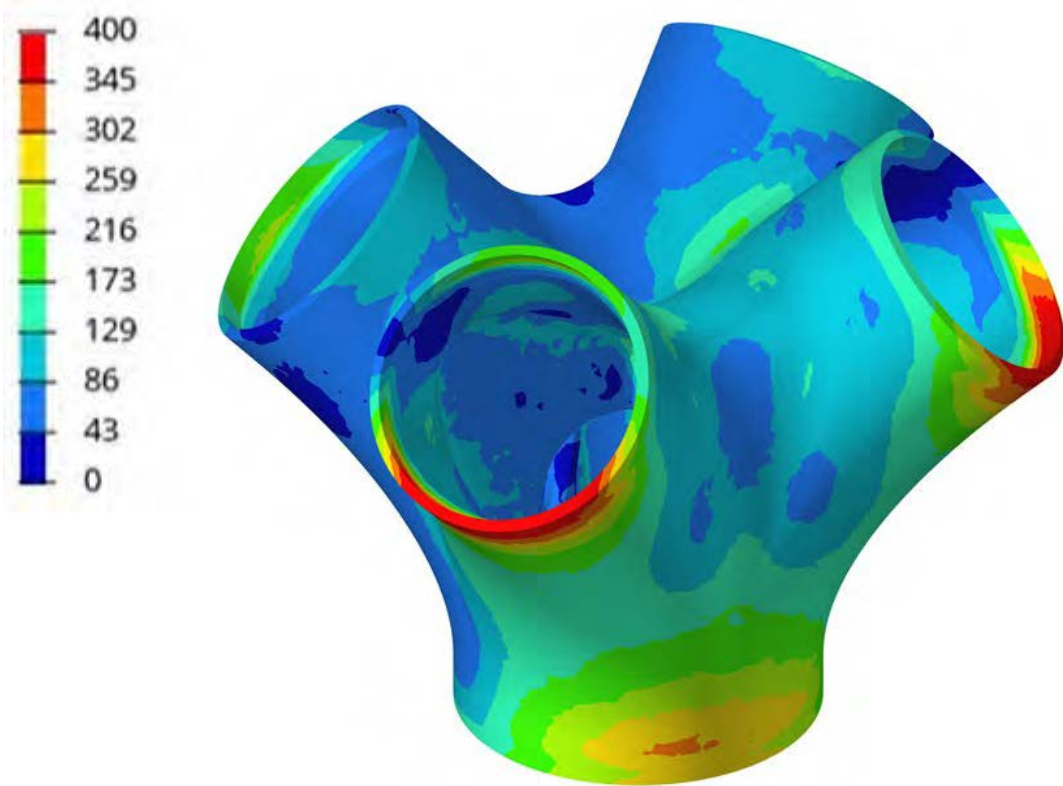
$$Utilization\ Factor = \frac{P_f}{P_r} + \frac{M_f}{M_r} = \frac{9919}{50975} + \frac{\sqrt{449.4^2 + 9151.1^2}}{16705} = 0.743 \leq 1.0$$



# DESIGN OF CAST STEEL NODES : TREE NODES

Von Mises stress contours (MPa)  
Max value = 350MPa

Plastic strain contours (mm/mm)  
Max value = 0.0024



# DESIGN OF CAST STEEL NODES : Y-NODES

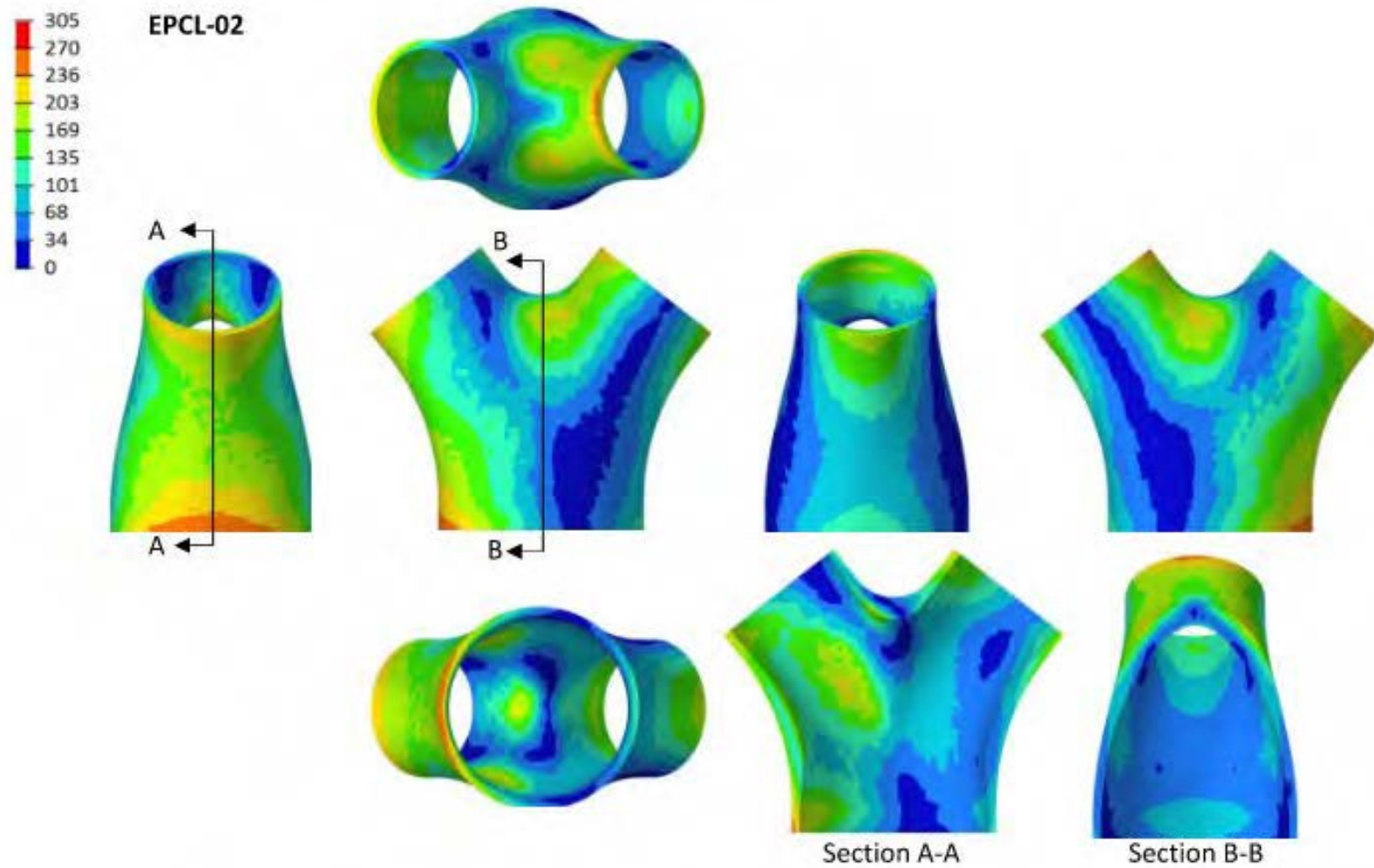
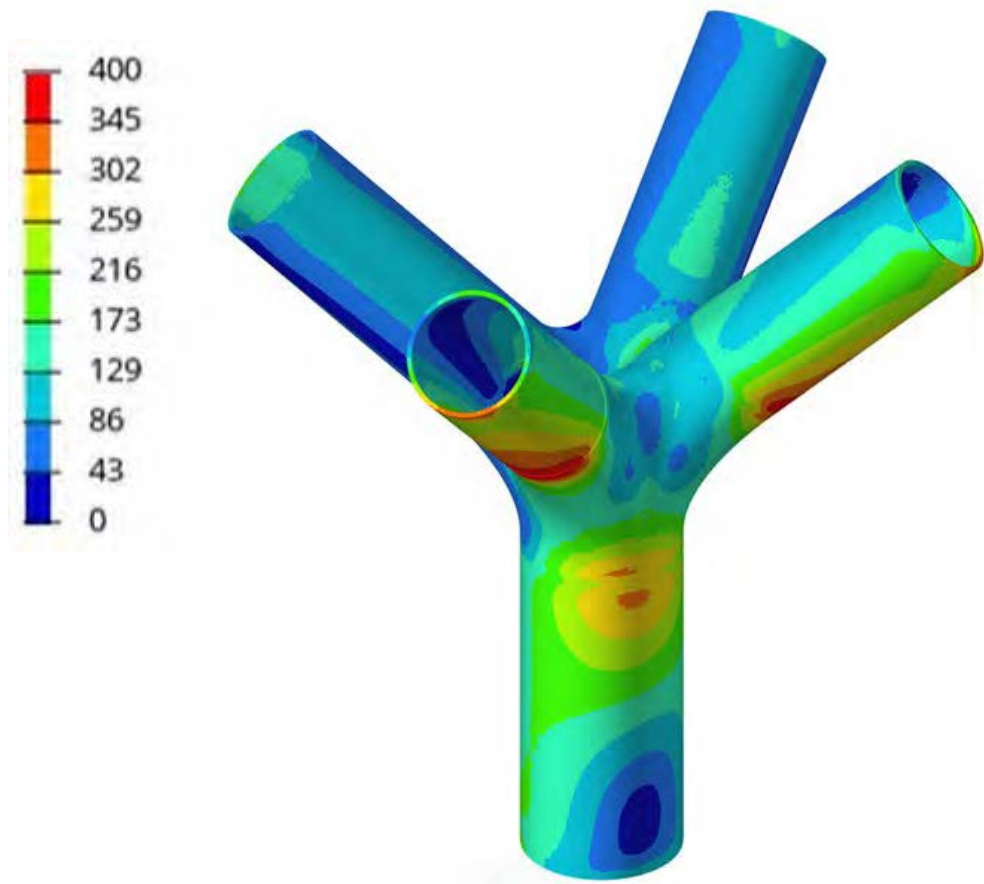


Figure 14. von Mises stress distribution of the EPCL-02 node (1.25D+1.25SD+1.5L) [MPa]

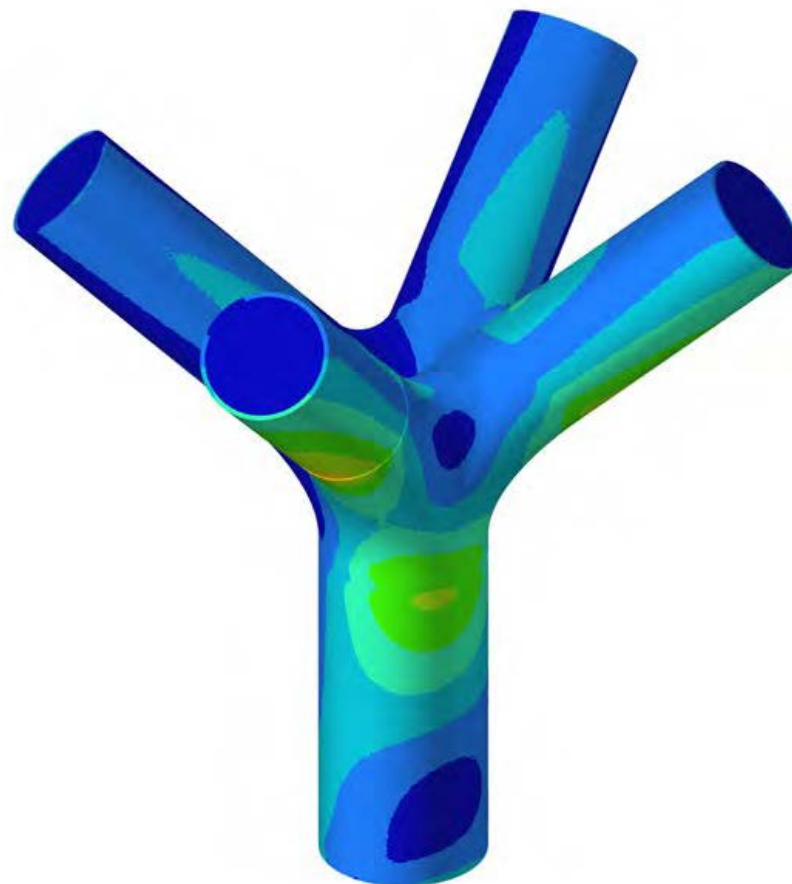


# UPPER & LOWER BOUND REVIEW

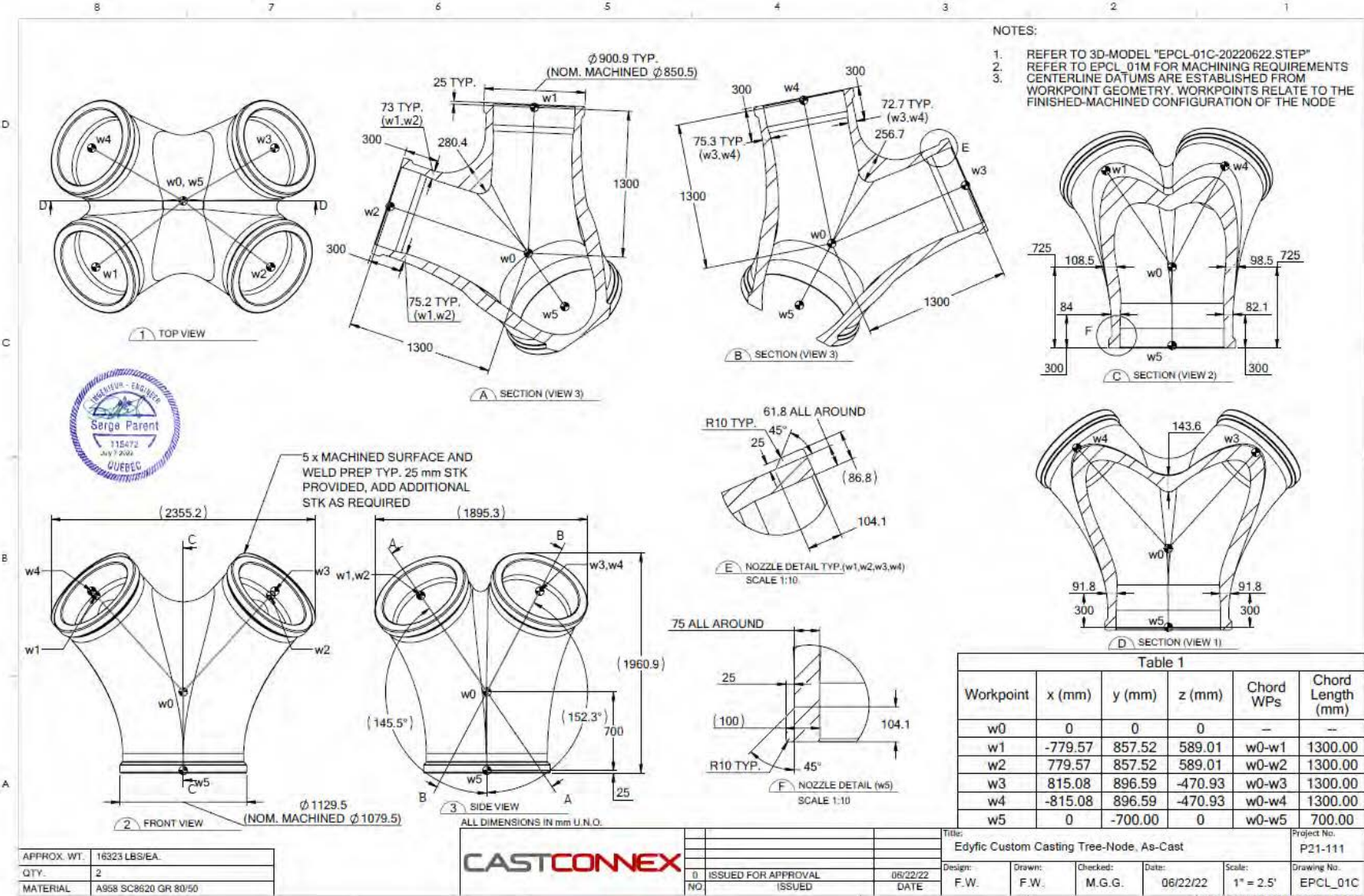
Simplified Concrete Bearing  
Von Mises stress contours (MPa)



Elastic "Concrete" Filling  
Von Mises stress contours (MPa)

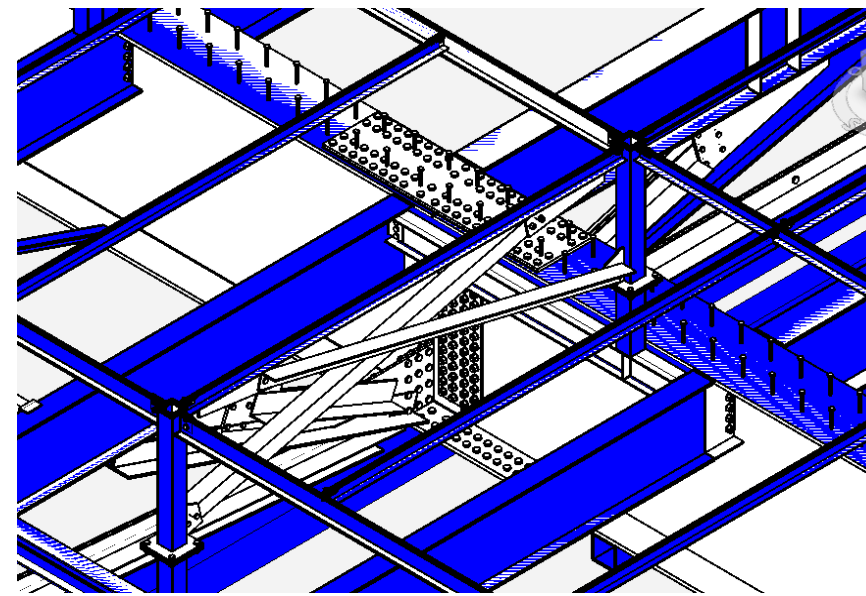
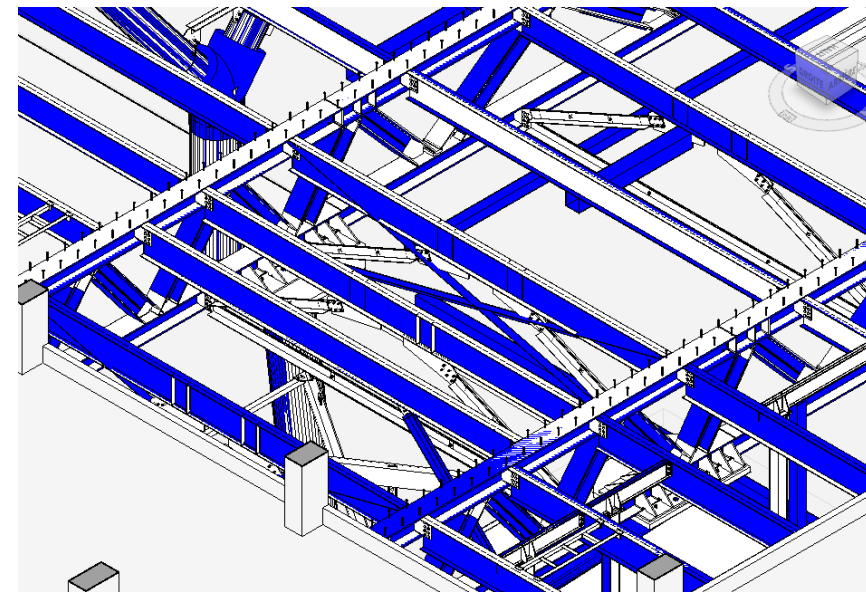
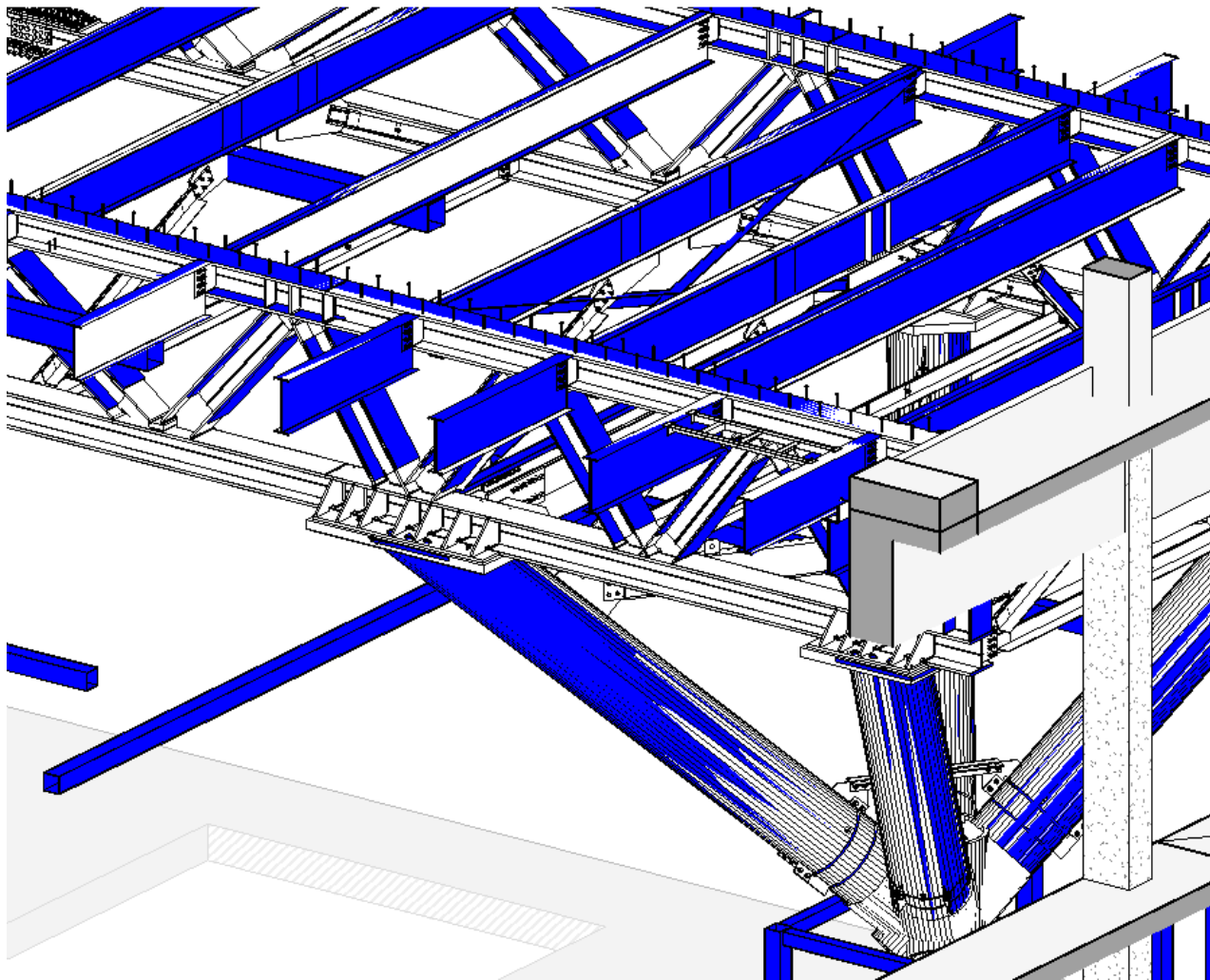


# CASTING SHOP DRAWINGS





# 3D MODEL COORDINATION





# MANUFACTURING & FABRICATION

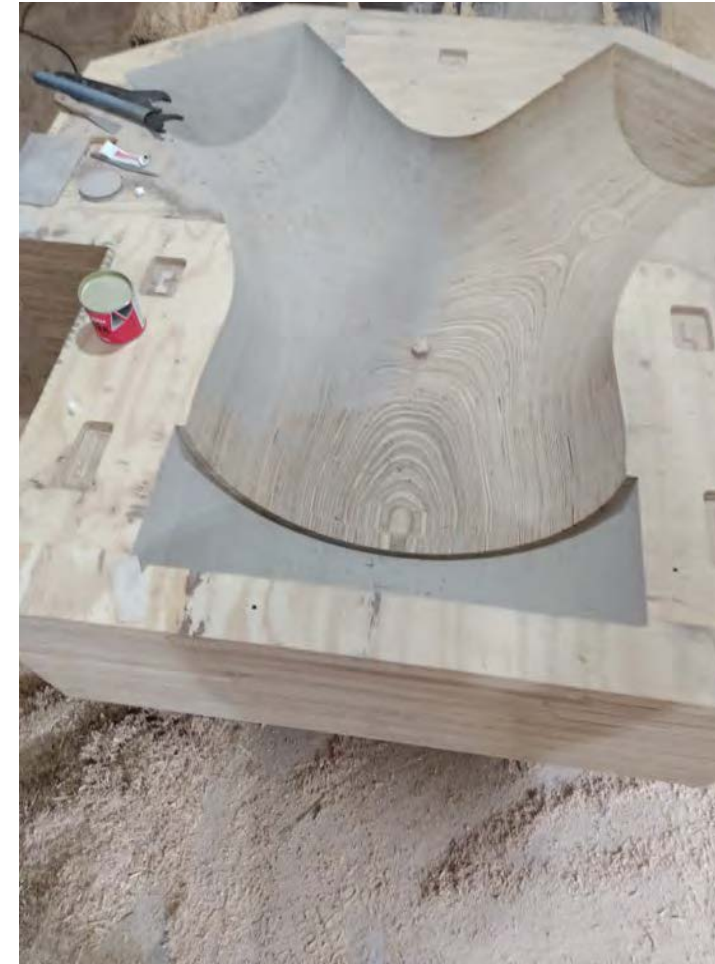


# CASTING PRODUCTION SPECIFICATION DEVELOPMENT



- 1) Stipulate production means and methods to the foundry  
Ex. Feeding, gating, riser locations, etc.
- 2) Select material grade for strength, toughness, weldability and ductility  
Ex. ASTM A958 Gr80/50
- 3) Set non-destructive examination methods and acceptance criteria  
Including Ultrasonic (UT), Magnetic Particle (MT), Radiographic (RT) & Visual
- 4) Establish as-cast and machining dimensional requirements and tolerances  
Shop drawings: as-cast drawing & machining print

# CASTING MANUFACTURING : PATTERN PRODUCTION

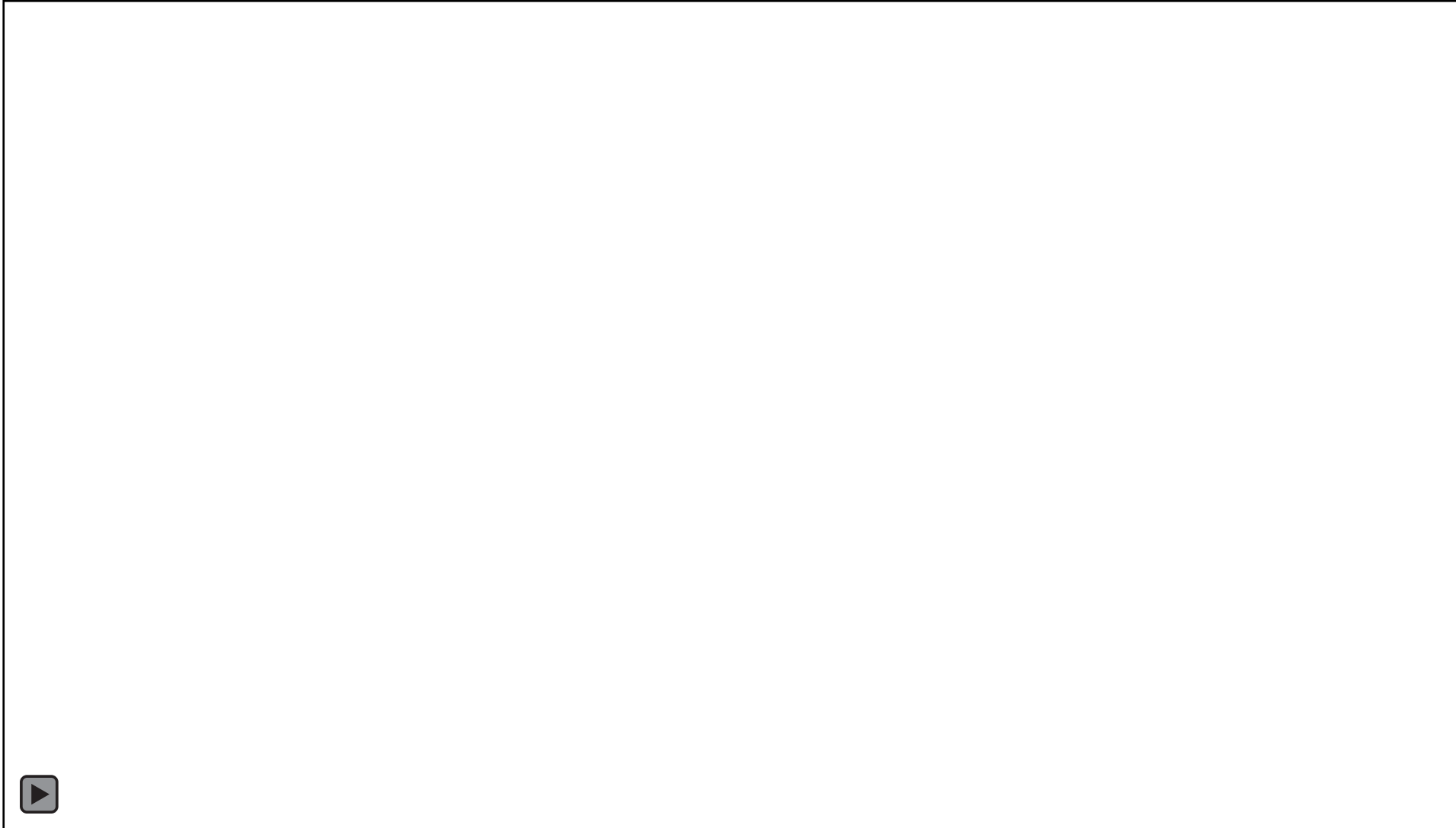




# CASTING MANUFACTURING : POUR, SHAKEOUT & FETTLING



# CASTING MANUFACTURING : MACHINING





# NON-DESTRUCTIVE EXAMINATION

Procedures include:

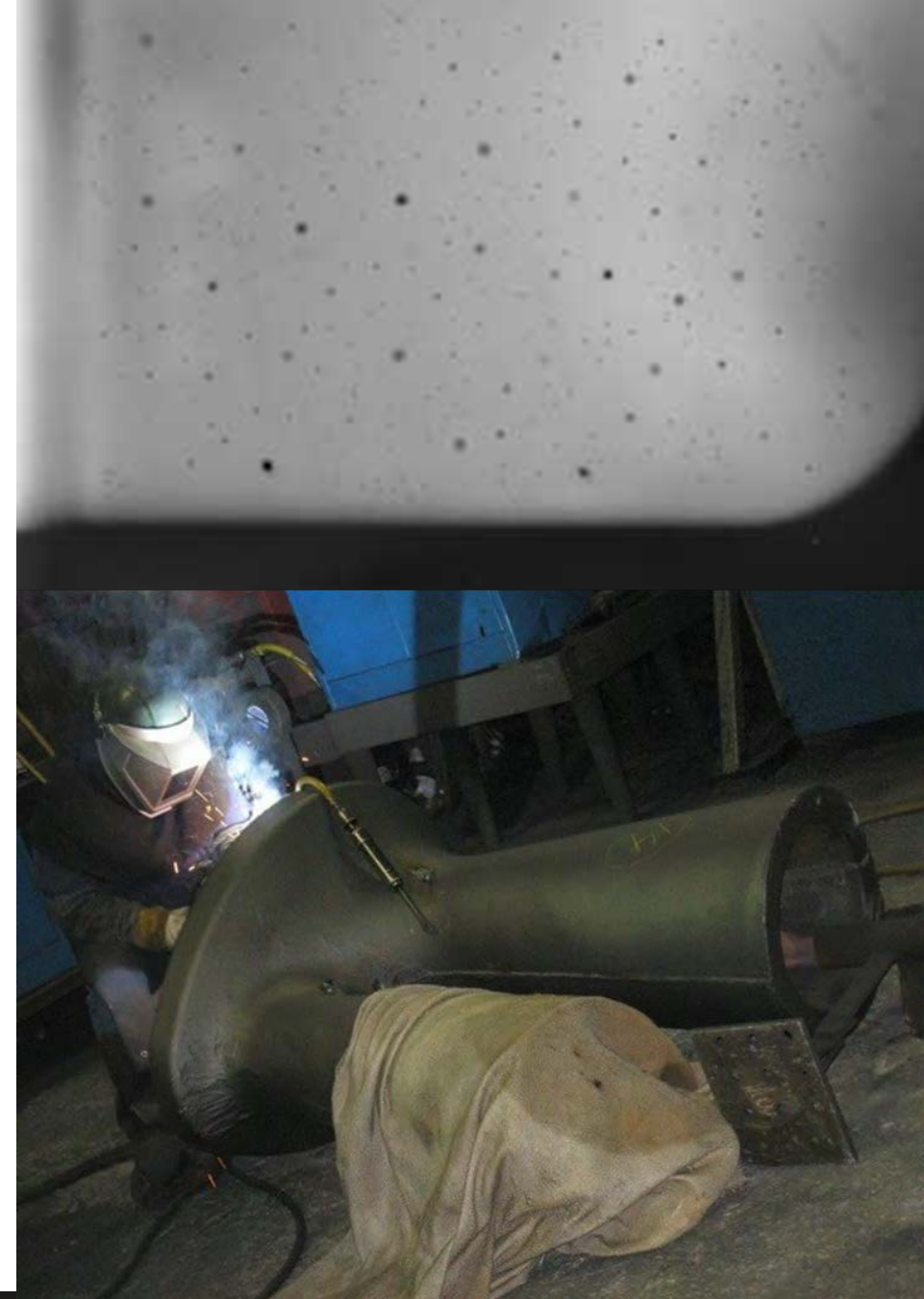
- Radiography Testing (RT)
- Ultrasonic Testing (UT)
- Magnetic Particle Inspection (MPI)
- Visual Examination

Predefined Acceptance Criteria (ASTM Standards)

- Based on predefined “levels”
  - Correlates to allowable indication size and distribution
    - Correlates to the structural efficacy of the casting

Areas that exceed acceptance criteria:

- Weld repaired
- Re-examined to confirm conformance to specification prior to final heat treat



# COMPLETED CASTINGS



**6 x Y-Nodes**

**OD x t (mm)**

Trunk

875x 28

Branch (2)

600 x 25



**2 x Tree Nodes**

**OD x t (mm)**

Trunk

1050 x 48

Branch (4)

850 x 32



# DELIVERING CASTINGS TO BEAUCE ATLAS



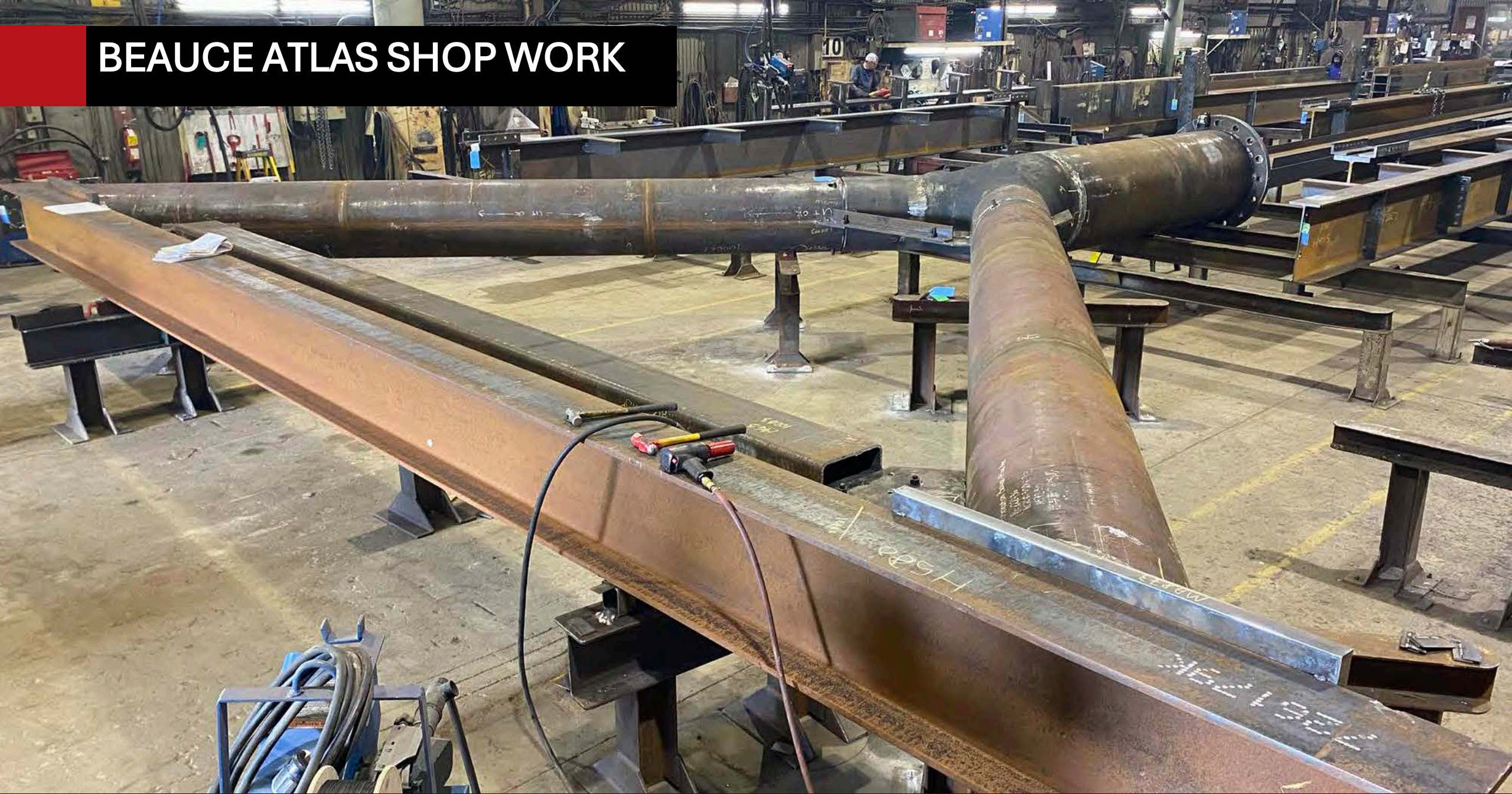


# BEAUCE ATLAST SHOP WORK





# BEAUCE ATLAS SHOP WORK



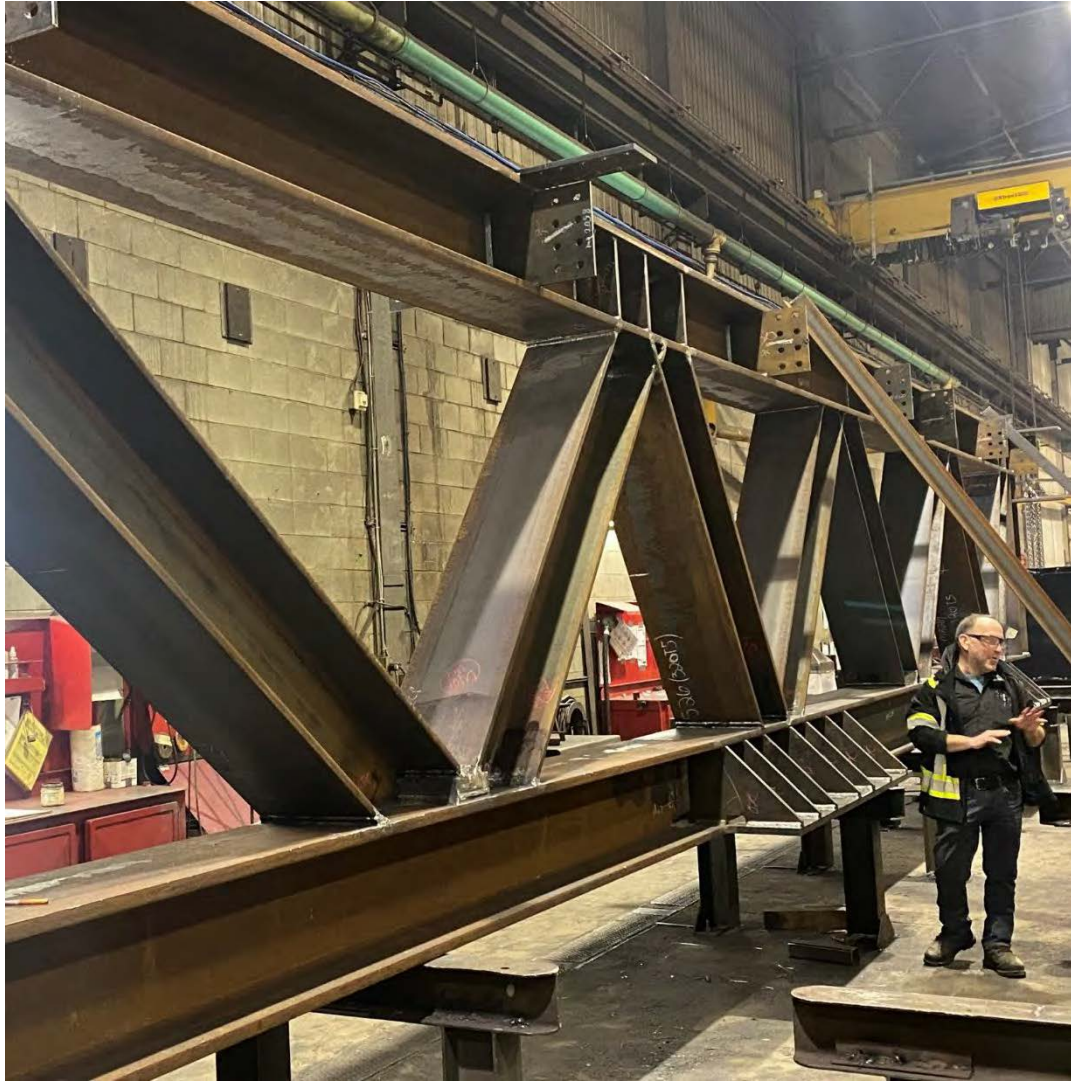


# BEAUCE ATLAS SHOP WORK





# BEAUCE ATLAS SHOP WORK





# FABRICATION YARD







# DELIVERY & SITE ERECTION

TO SITE





# TO SITE





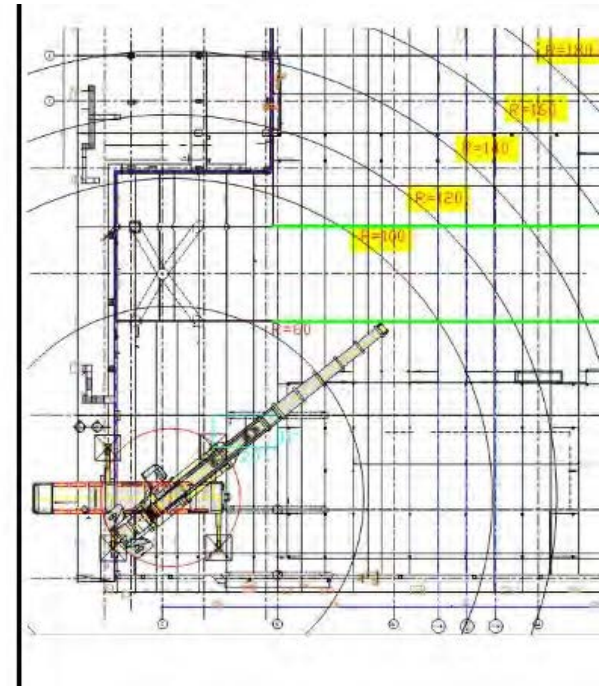
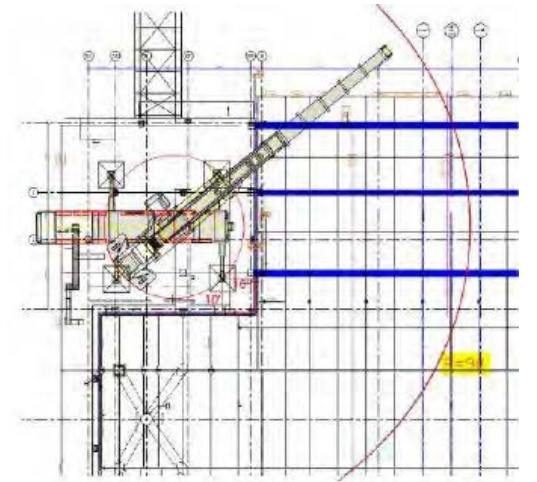
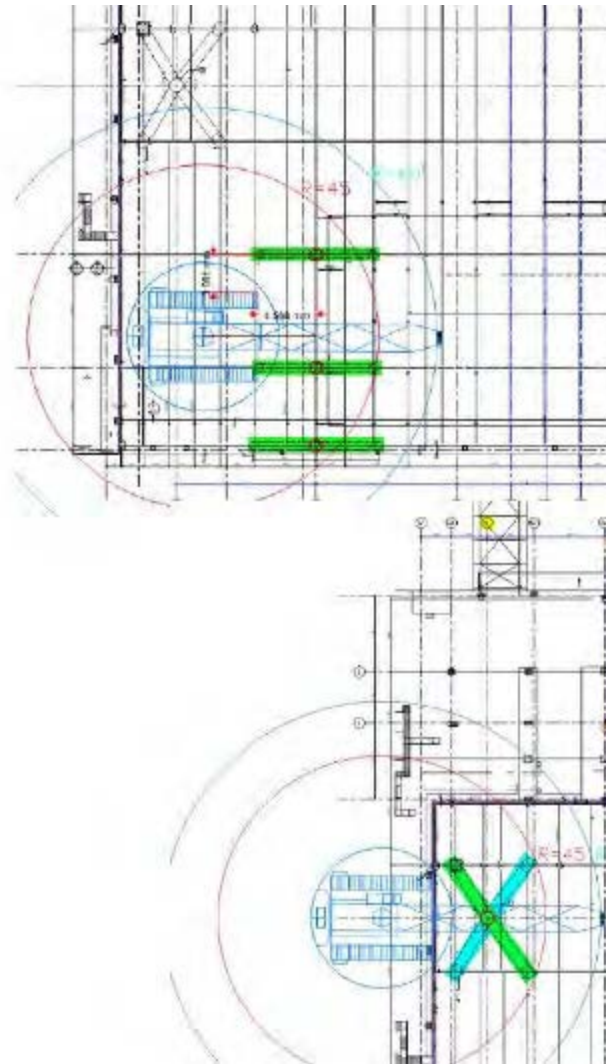
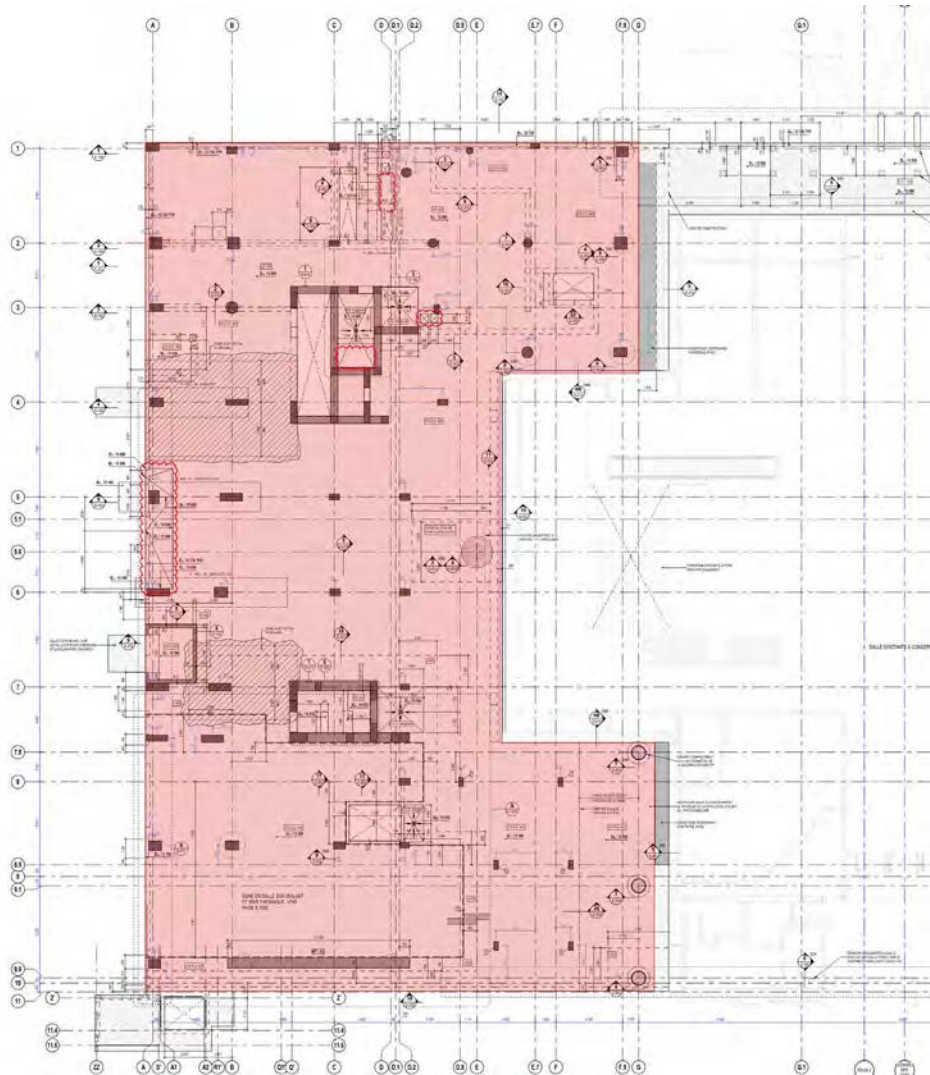
# ON SITE





# CRANE WORK

650T mobile crane + 250T Crawler



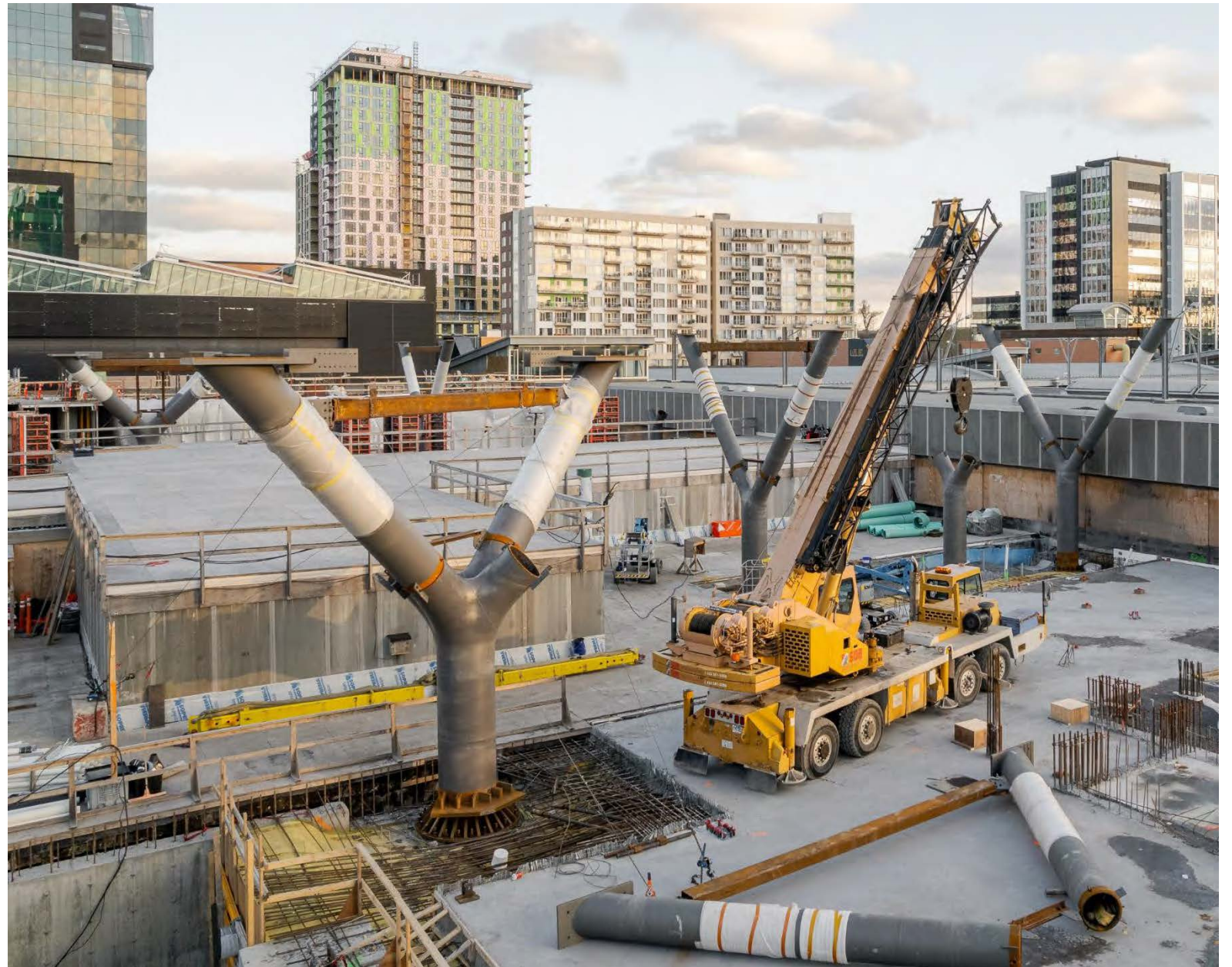


# SITE WORK





# SITE WORK



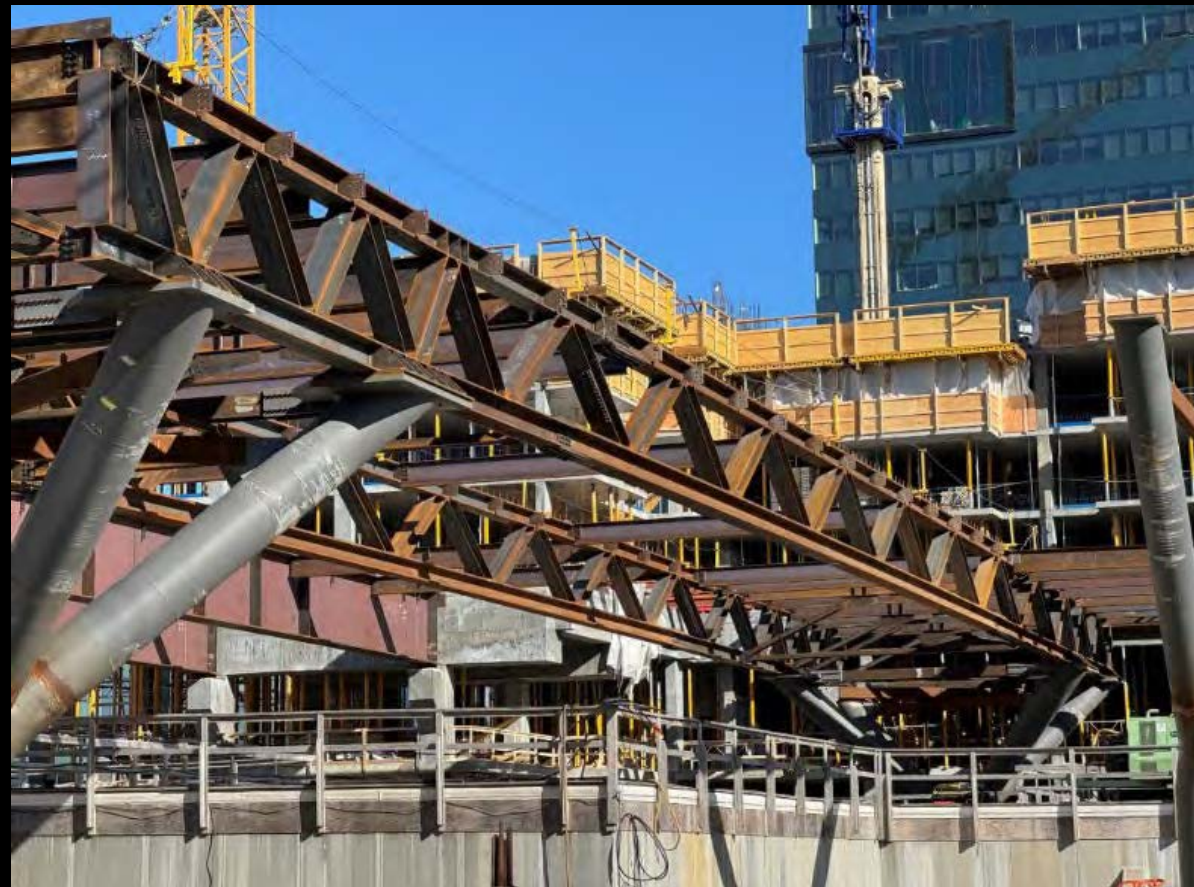
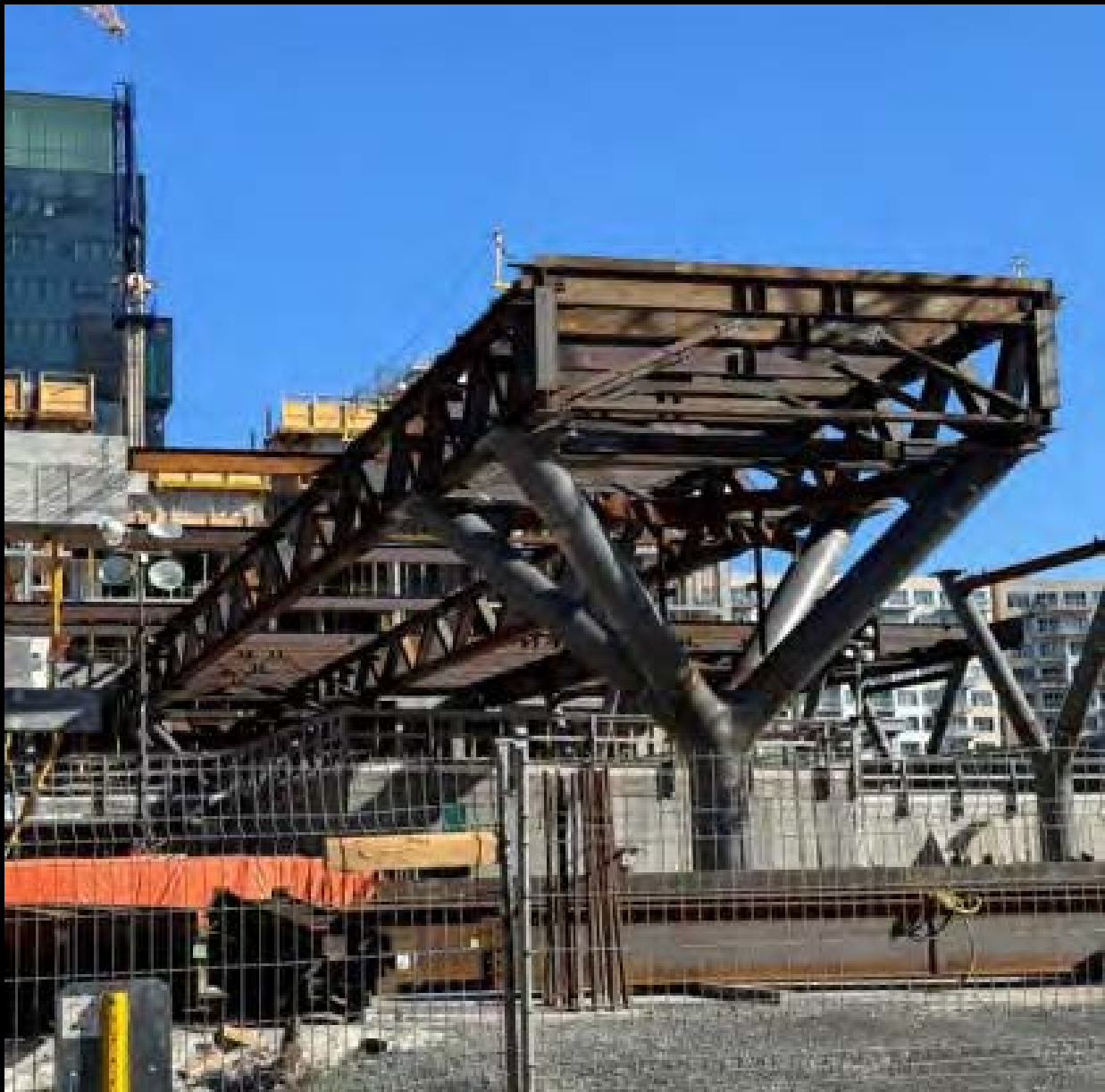




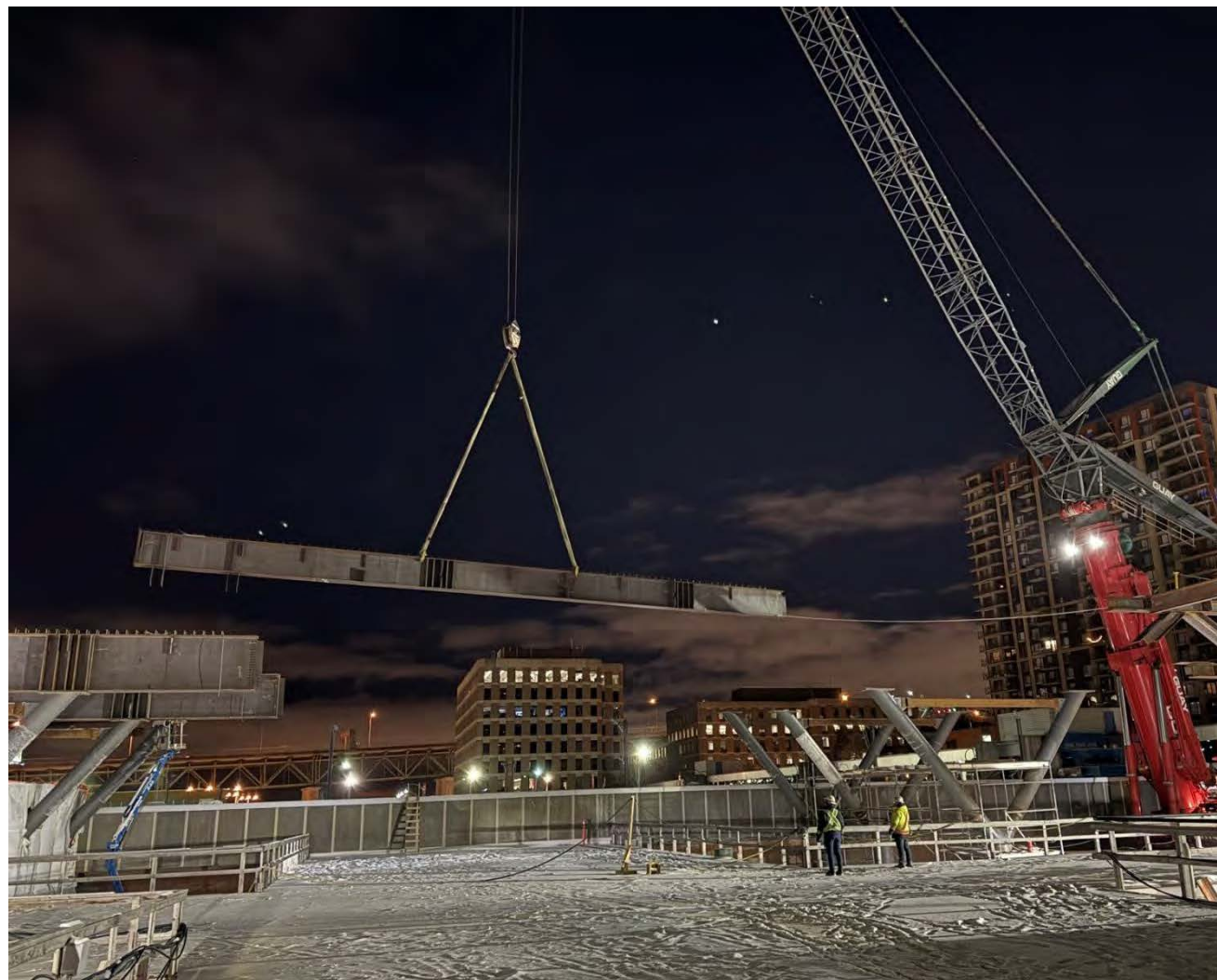


















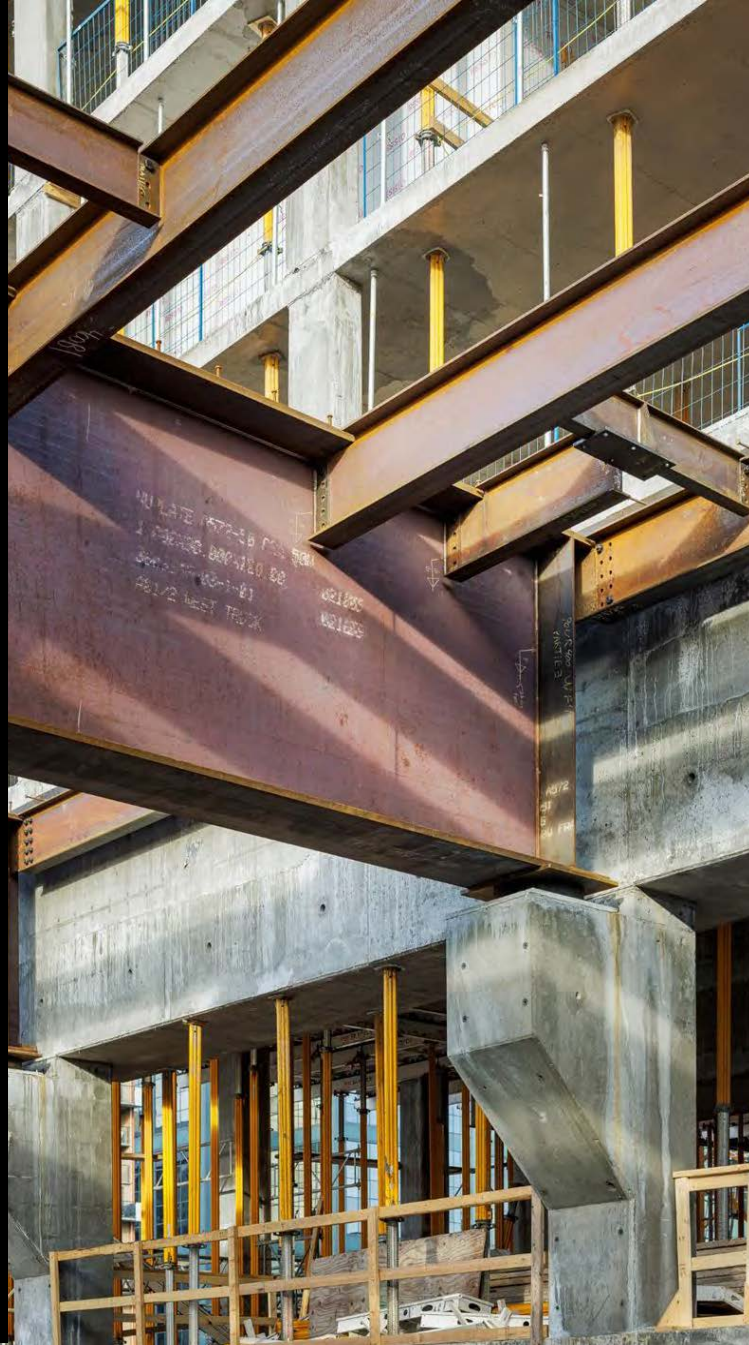
























# FROM CONCEPT TO REALITY







# Evolution of Structures

Steel Castings in the Eye of the Design Team

**CASTCONNEX<sup>®</sup>**  
innovative components for inspired designs

## THANK YOU!

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